



NIZHNY NOVGOROD STATE TECHNICAL UNIVERSITY
N.A. R.E. ALEKSEEV



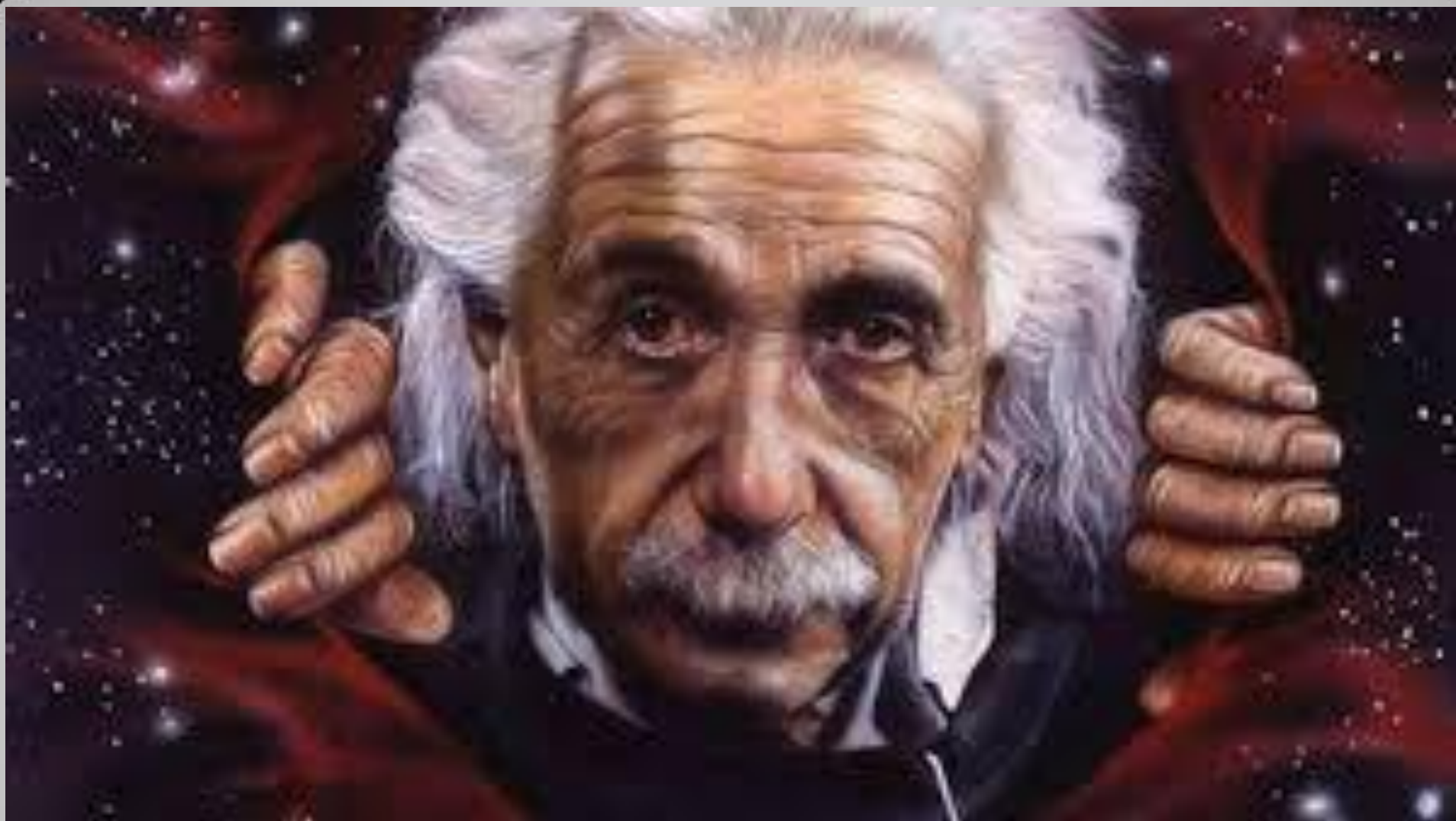
Химики без границ

Prof. Ilya V. Vorotyntsev

Nanotechnology and
Biotechnology
Department



Laboratory of Membrane and Catalytic Processes



Окружающий Мир это дружественная или враждебная среда?

Почему мы боимся химии?

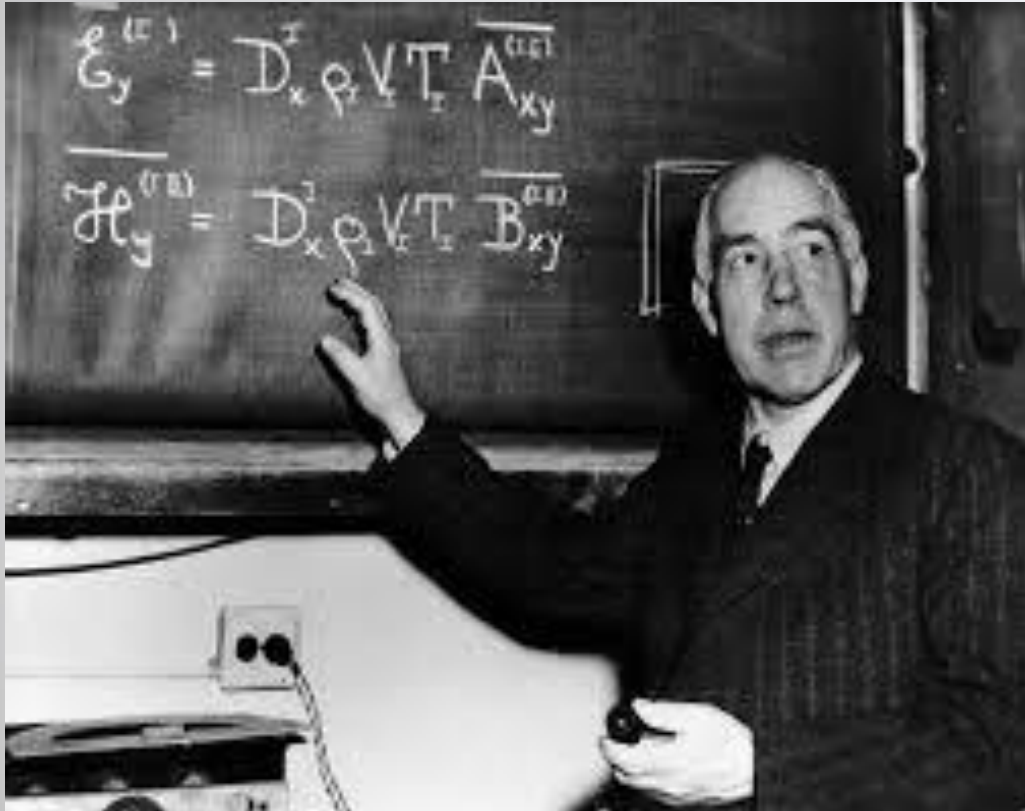


Почему мы боимся химии?

КИНО СБОРКИ



Нильс БОР



- На свете есть столь серьезные вещи, что говорить о них можно только шутя...

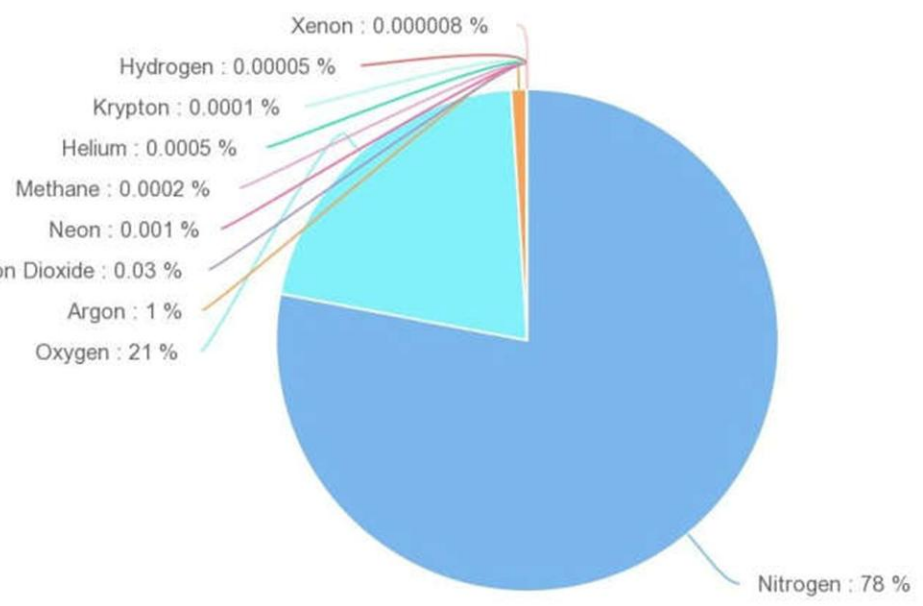
Химия вокруг нас...



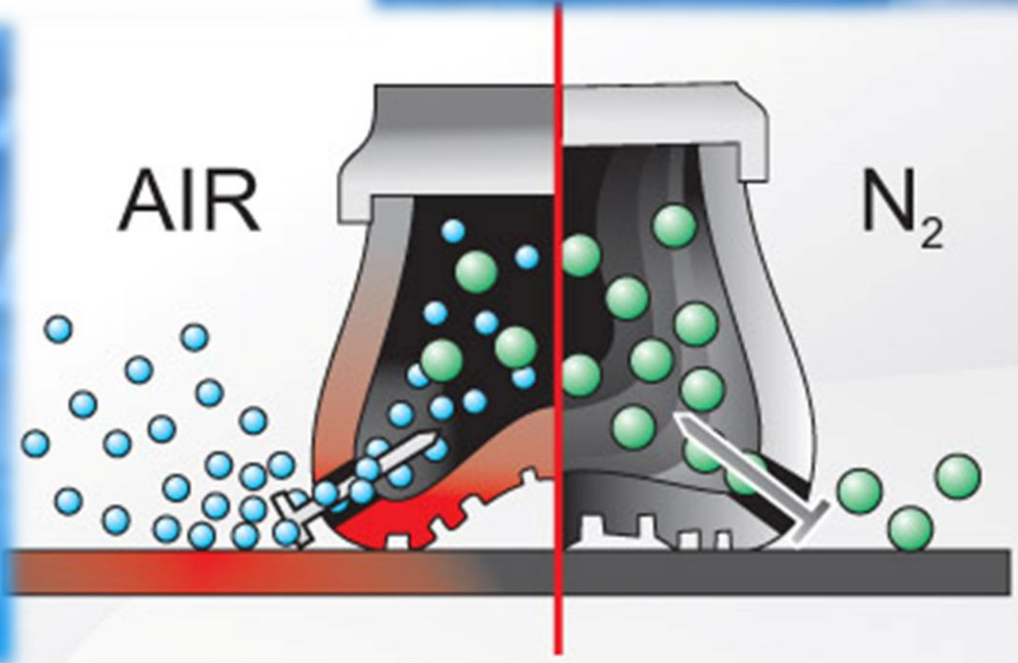
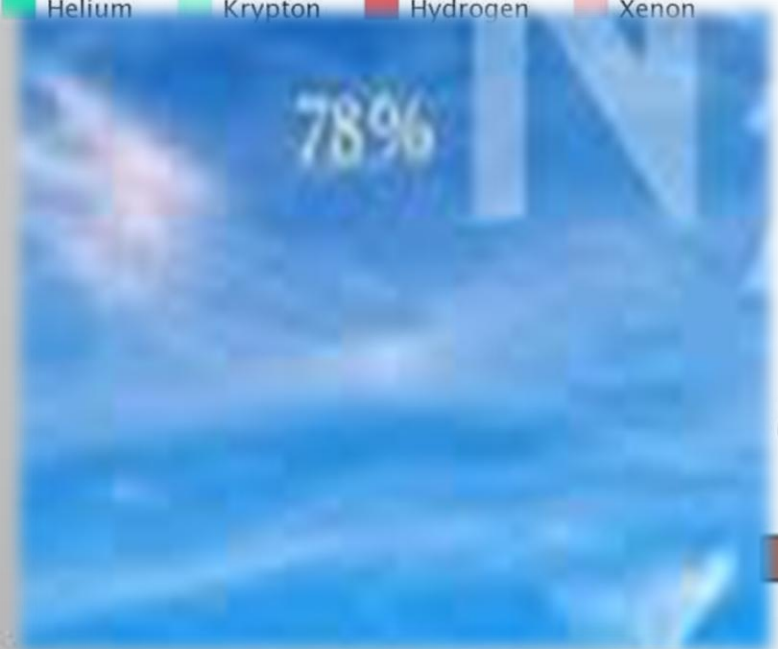
Всё, что нас окружает – это химия!

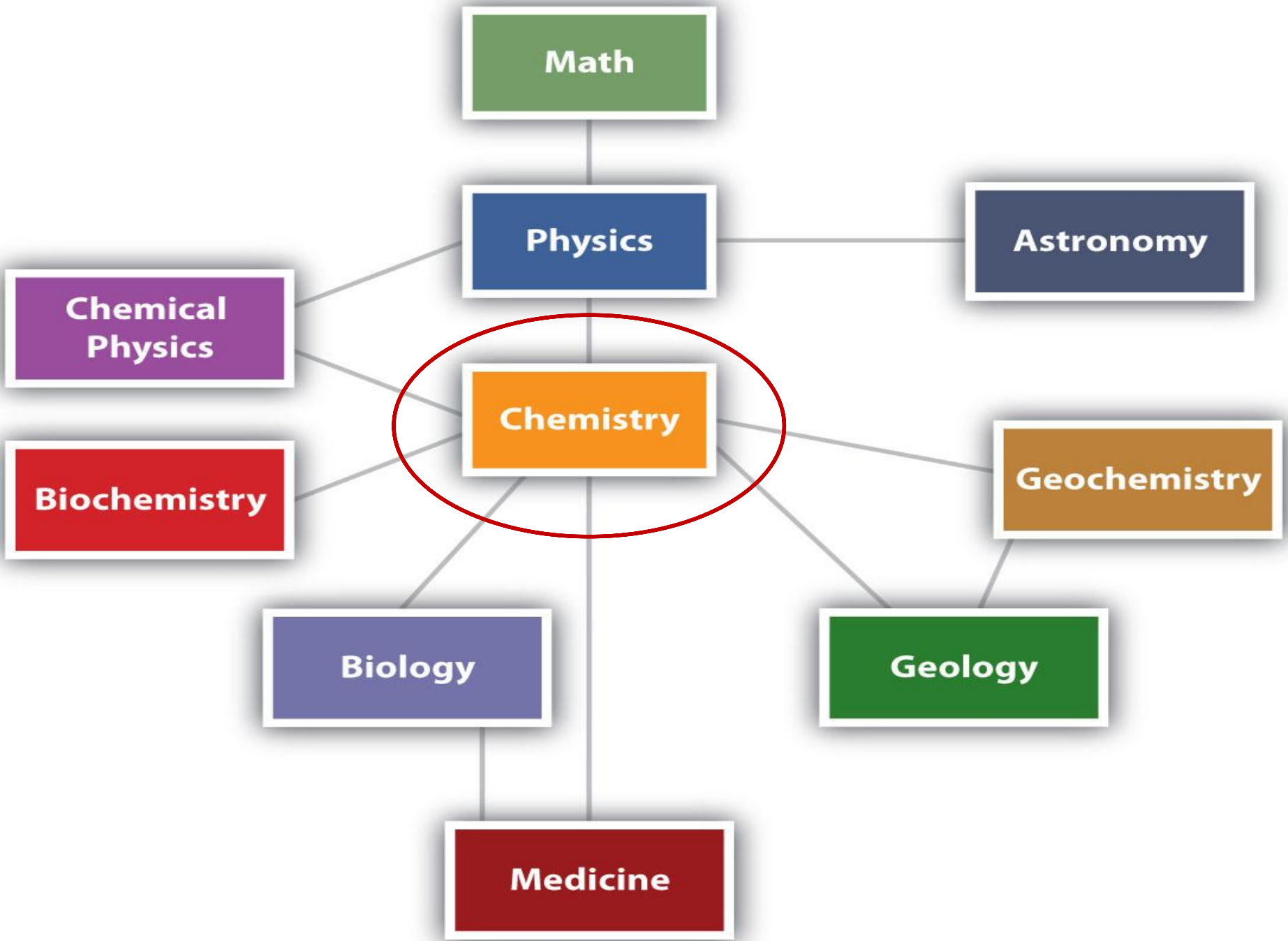


AIR COMPOSITION



- Nitrogen
- Oxygen
- Argon
- Carbon Dioxide
- Neon
- Methane
- Helium
- Krypton
- Hydrogen
- Xenon





Math

Physics

Astronomy

Chemical Physics

Chemistry

Geochemistry

Biochemistry

Biology

Geology

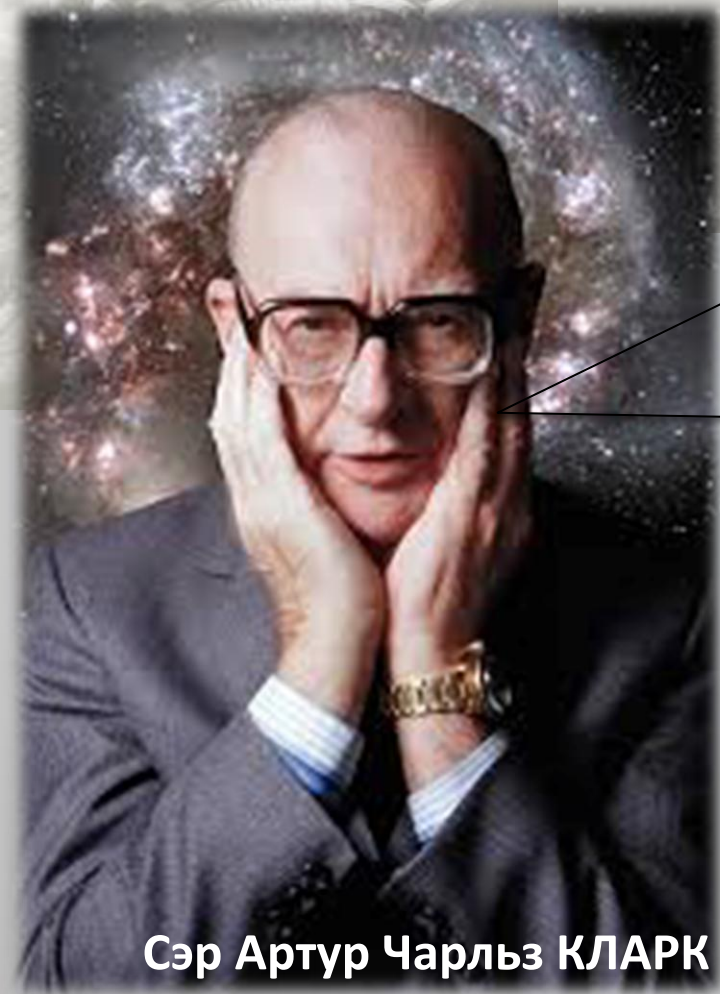
Medicine



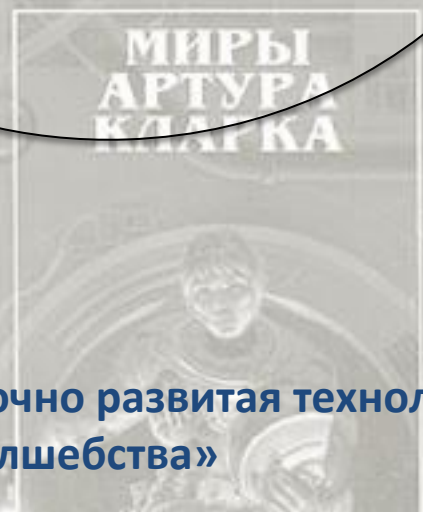
Артур Кларк
Конец детства



Any sufficiently advanced technology is indistinguishable from magic*



Сэр Артур Чарльз КЛАРК



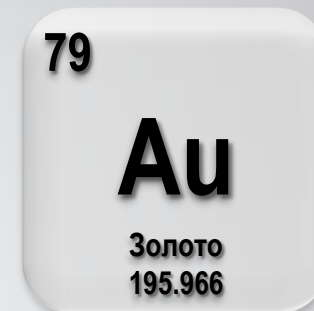
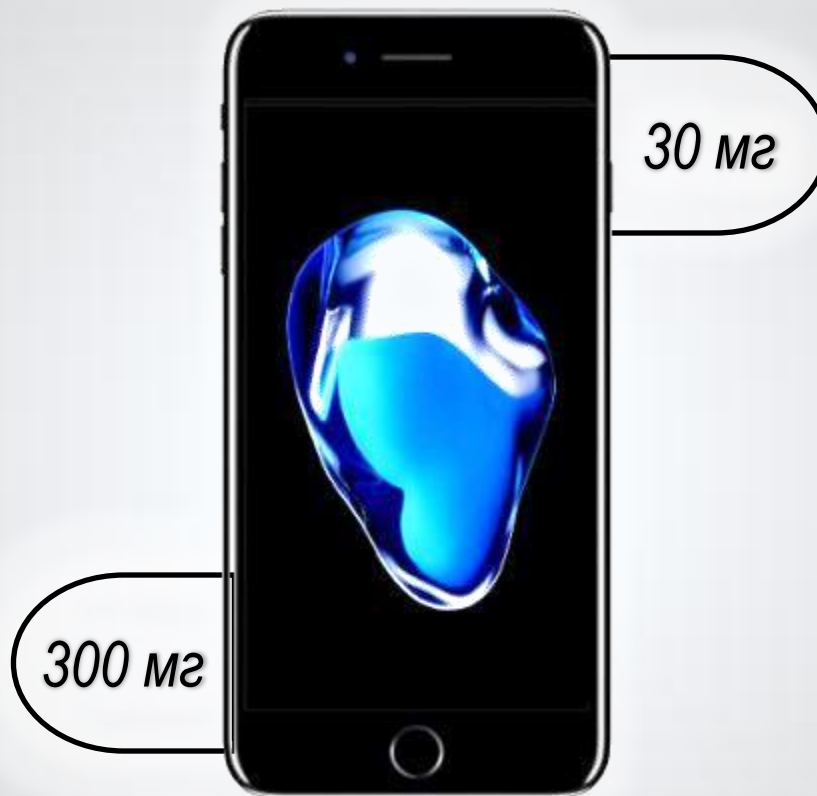
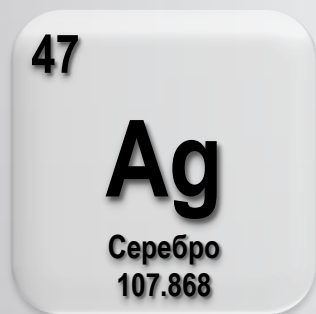
* «Любая достаточно развитая технология неотличима от волшебства»

Электроника – неотъемлемая часть нашей жизни!

Электроника – «мозг и нервная система» высокотехнологичных изделий всех отраслей мировой индустрии!



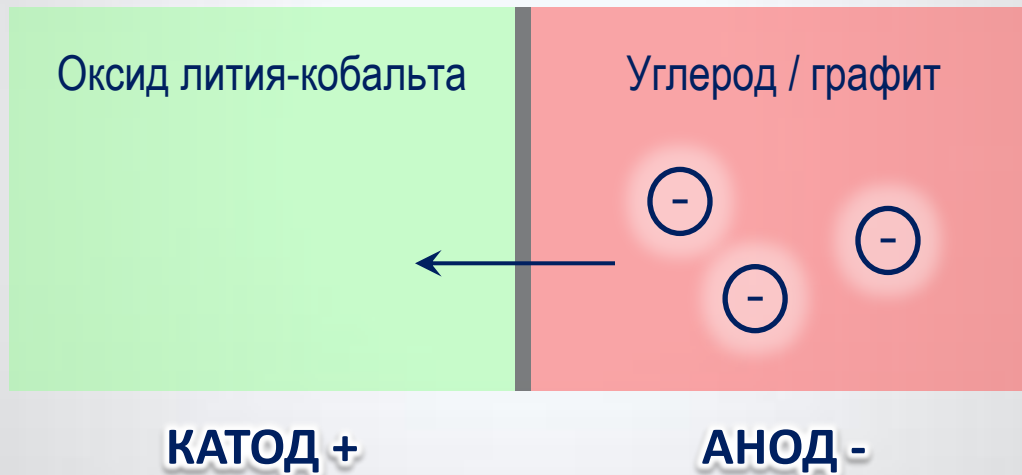
Повседневная химия



Сайт кафедры «Нанотехнологии и биотехнологии»
<http://www.nntu.ru/nbt>



Повседневная химия



Сайт кафедры «Нанотехнологии и биотехнологии»
<http://www.nntu.ru/nbt>



Повседневная химия

59

Pr

Празеодим
140.908

65

Tb

Тербий
158.925



39

Y

Иттрий
88.906

64

Gd

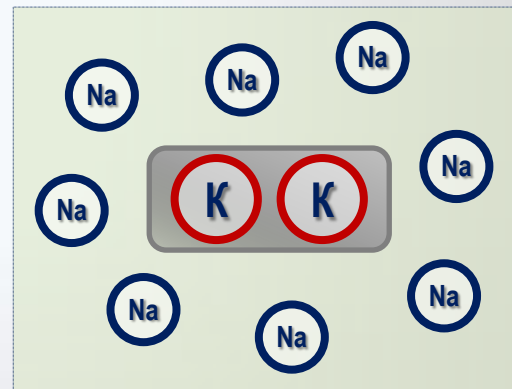
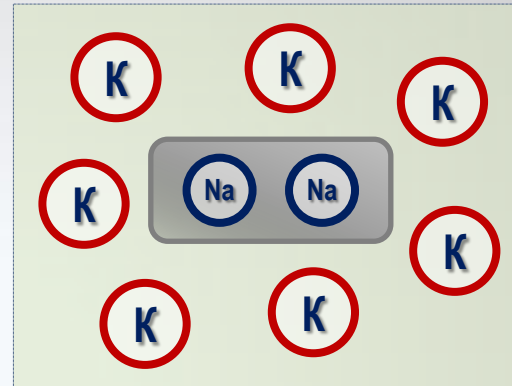
Гадолиний
157.253



Сайт кафедры «Нанотехнологии и биотехнологии»
<http://www.nntu.ru/nbt>



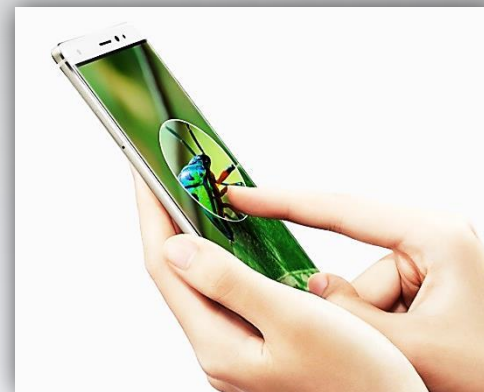
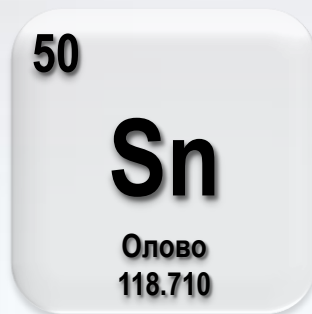
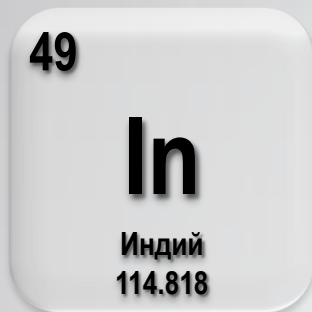
Повседневная химия



Сайт кафедры «Нанотехнологии и биотехнологии»
<http://www.nntu.ru/nbt>



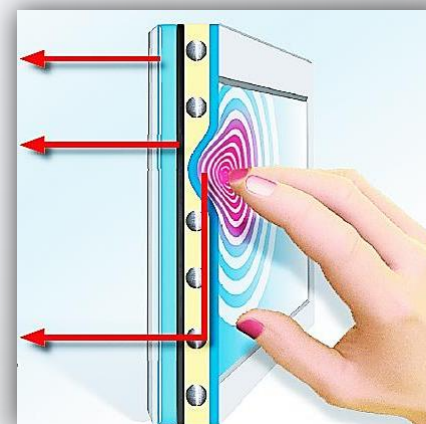
Повседневная химия



Токопроводящий слой

Второй токопроводящий слой на
минимальном расстоянии

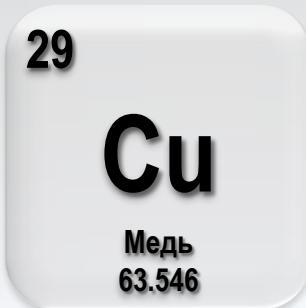
При прикосновении слои соприкасаются,
и возникает слабый ток



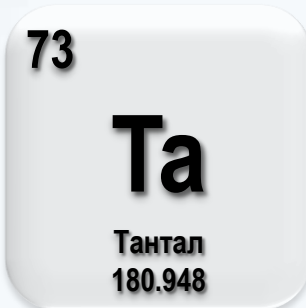
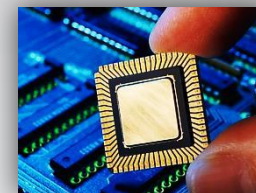
Сайт кафедры «Нанотехнологии и биотехнологии»
<http://www.nntu.ru/nbt>



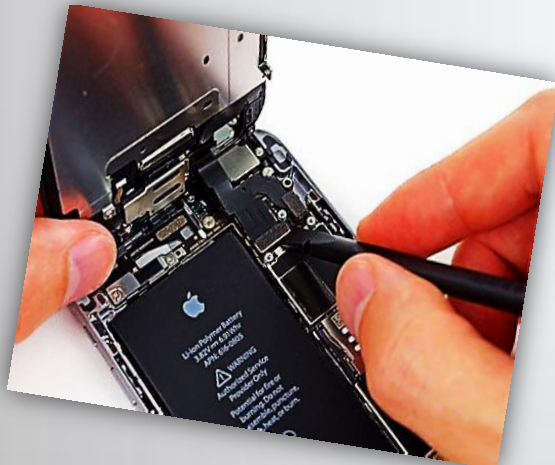
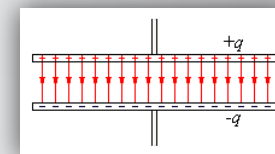
Повседневная химия



➔ Металлизация



➔ Конденсаторы

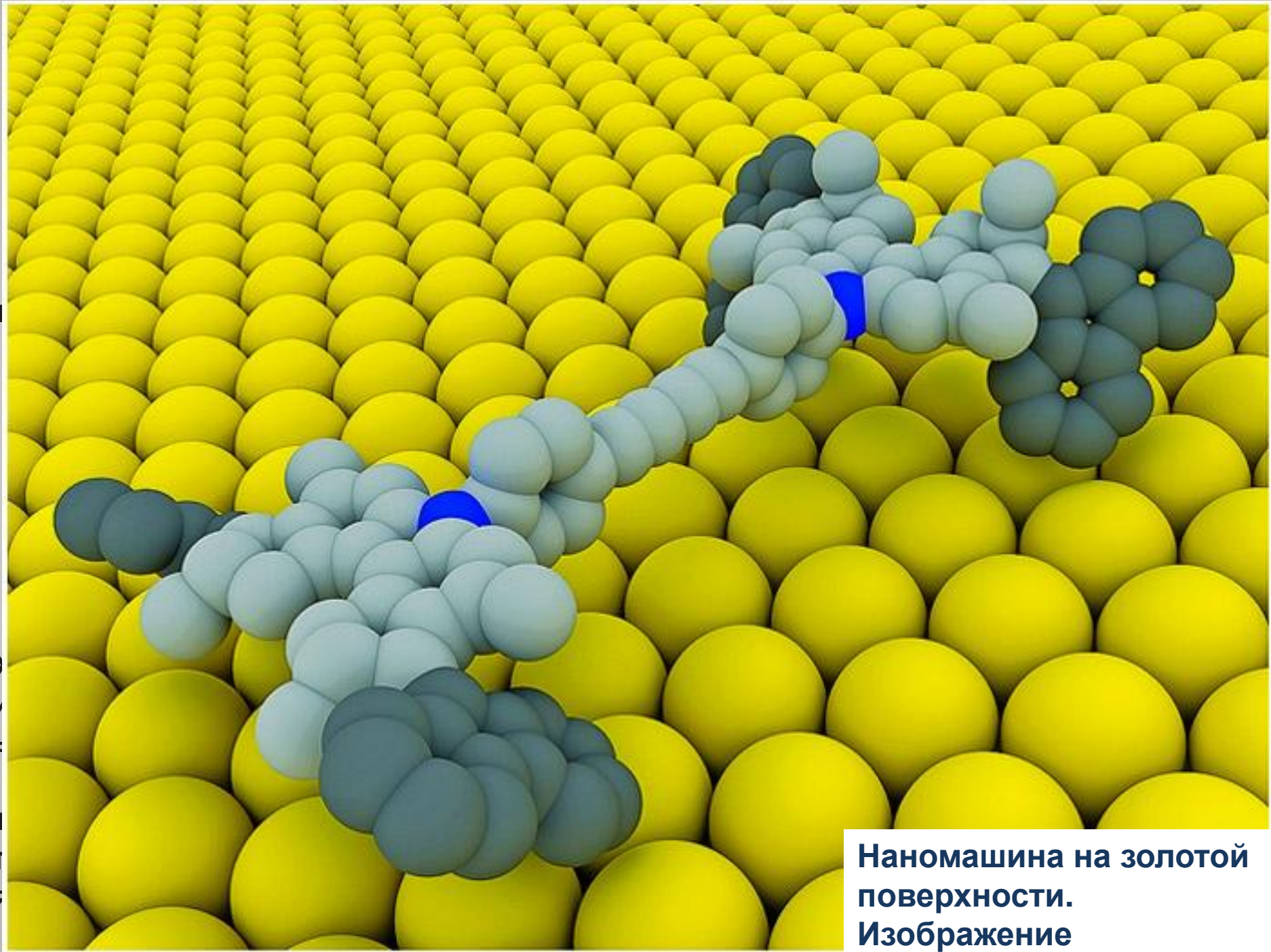


➔ Мозг всей системы!



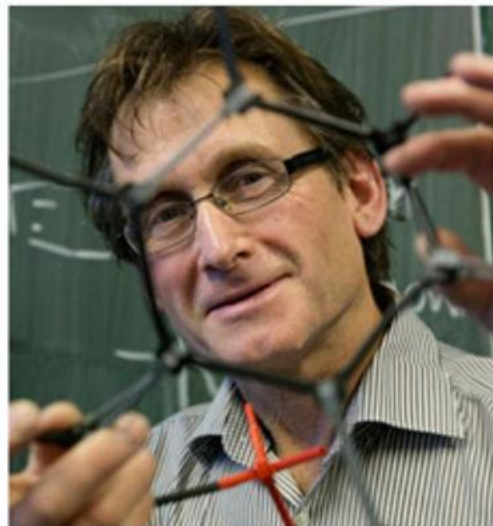
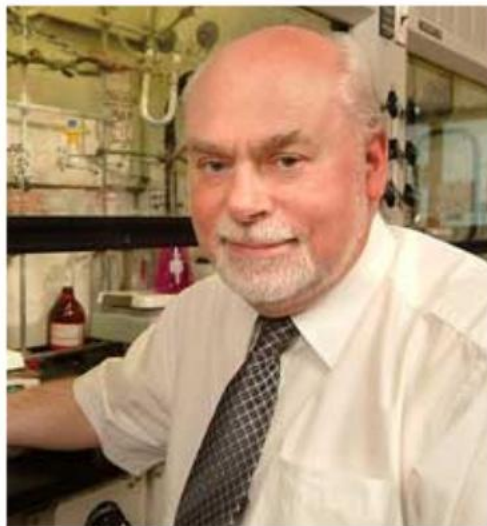
Сайт кафедры «Нанотехнологии и биотехнологии»
<http://www.nntu.ru/nbt>



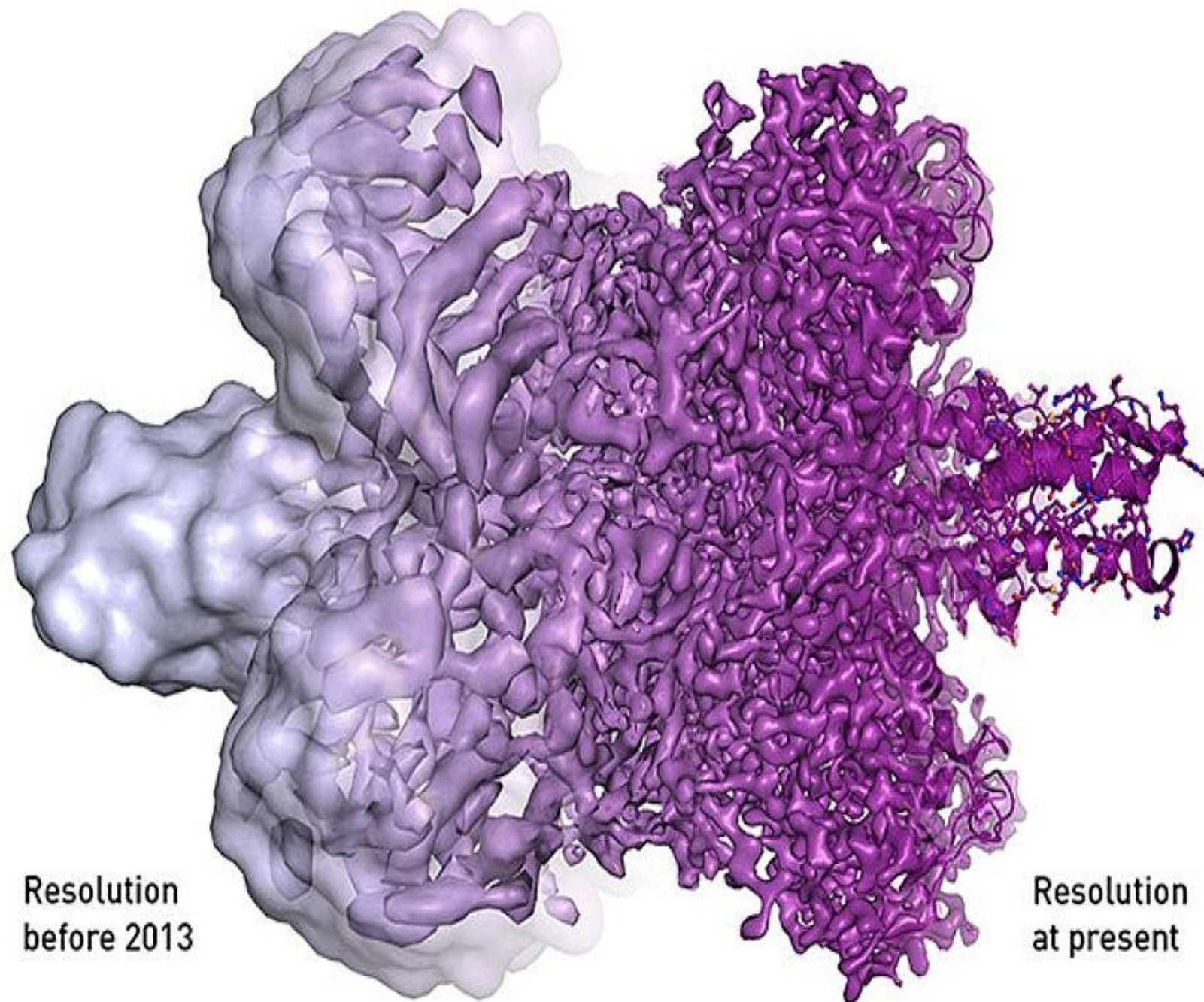


Наномашина на золотой поверхности. Изображение

Nobel Prize 2016



Лауреаты Нобелевской премии по химии 2016 года: Жан-Пьер Соваж (Jean-Pierre Sauvage), Фрейзер Стоддарт (J. Fraser Stoddart), и Бернард Феринга (Bernard L. Feringa). Изображение с сайта cen.acs.org



Nobel Prize 2017



Рис. 1. Лауреаты Нобелевской премии по химии 2017 года. Слева направо: Жак Дюбоше, Йоахим Франк и Ричард Хендерсон. Фото с сайта sciencenews.org

НЕ НОБЕЛЕВСКИЙ ЛАУРЕАТ

Не придумывал я водку!
Я ученый, а не бармен!



1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
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1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
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Общий рейтинг

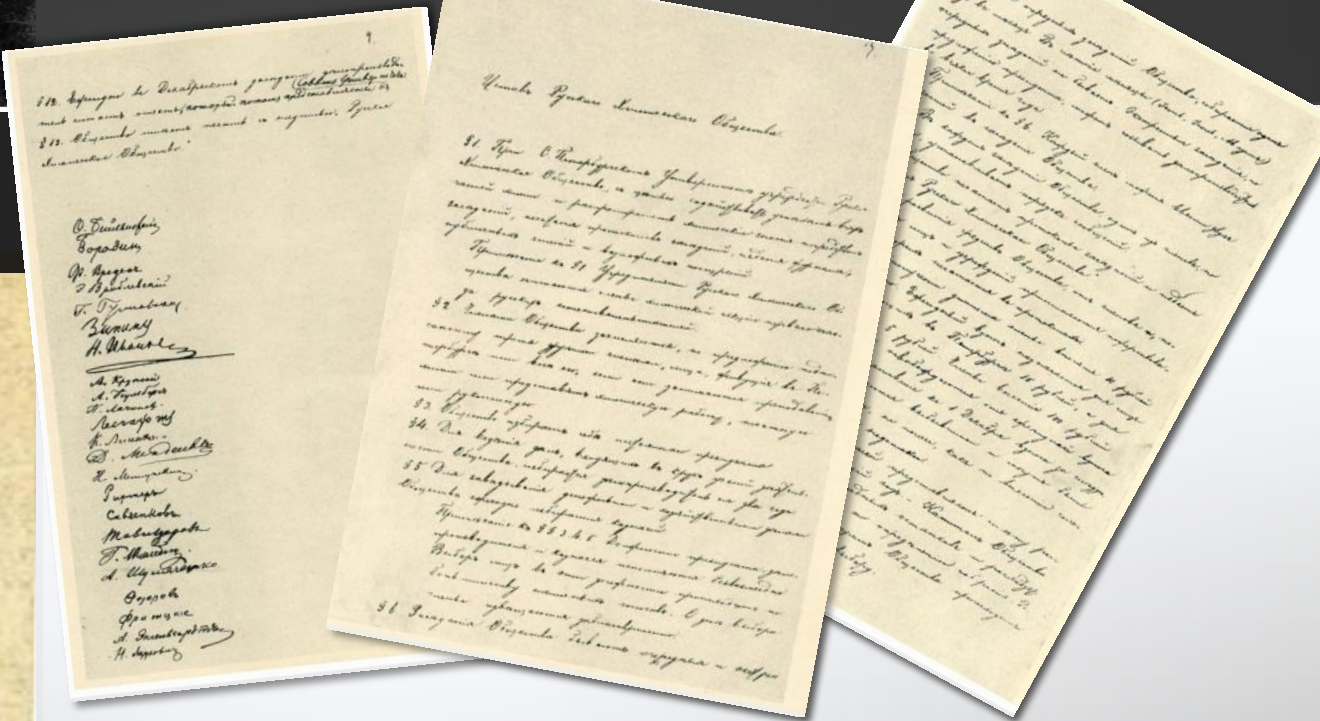
	всего голосов	место
Александр Невский	524 575	1
П.А. Столыпин	523 766	2
И.В. Сталин	519 071	3
А.С. Пушкин	516 608	4
Петр I	448 857	5
В.И. Ленин	424 283	6
Ф.М. Достоевский	348 634	7
А.В. Суворов	329 028	8
Д.И. Менделеев	306 520	9
Иван IV Грозный	276 570	10
Екатерина II	152 306	11
Александр II	134 622	12

RUSSIAN CHEMICAL SOCIETY n.a. D. I. Mendeleev

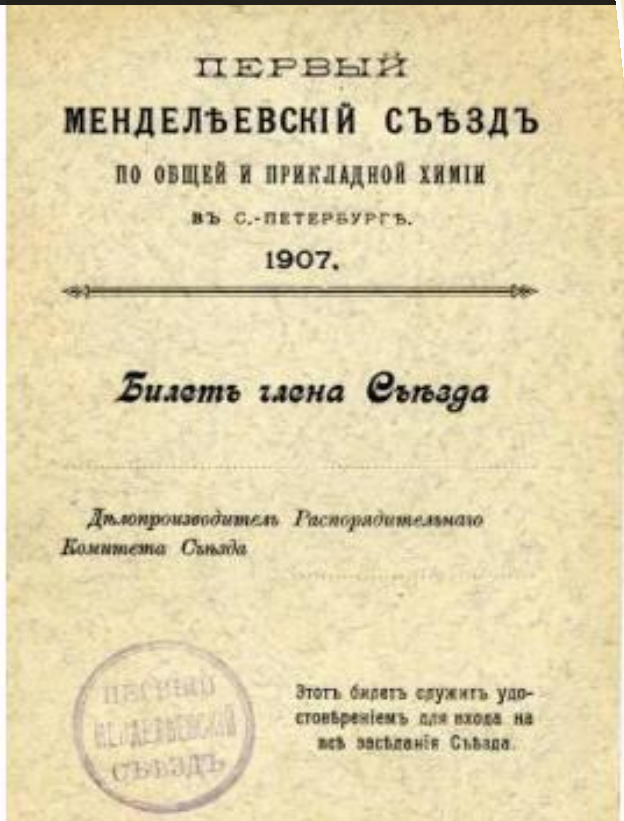


January 1868

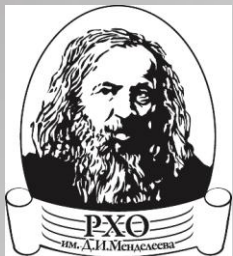
The first congress of Russian naturalists



February 1868 - sketch of the main provisions of the Charter



1907 - the first Mendeleev Congress on General and Applied Chemistry



NUMBER OF MEMBERS OF THE RUSSIAN CHEMICAL SOCIETY





YOUTH COMMUNITY

**A NEW STAGE OF
CHEMICAL SOCIETY
n. a. D. I. Mendeleev**



Together
with
the whole
planet!



40 000 PARTICIPANTS
FROM **188** COUNTRIES







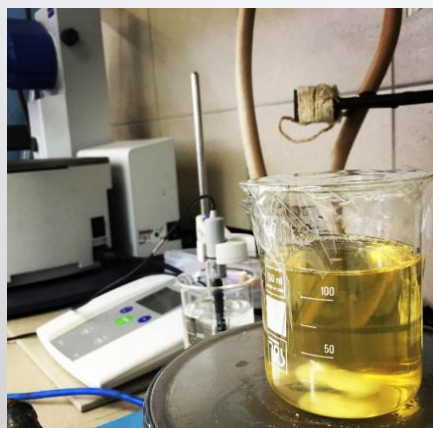
IYCN





WELCOME

Laboratory of membrane
and catalytic processes



www.lmcp.today

604050, Nizhny Novgorod,
Minina Street, 24

Meet Our team

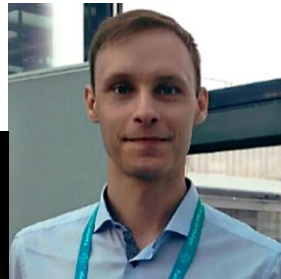
Professional. International. Innovative



Prof. Ilya V. Vorotyntsev



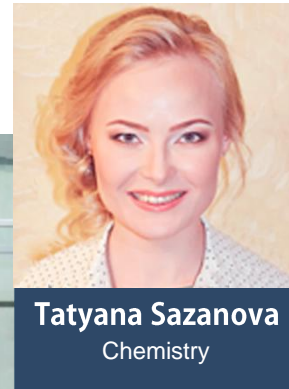
Anton Petukhov
Chemical Technology



Maxim Trubyanov
Chemical Technology



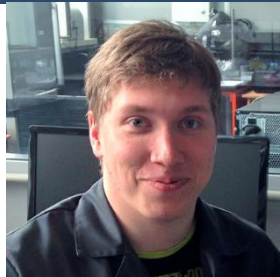
Andrey Vorotyntsev
Chemistry



Tatyana Sazanova
Chemistry



Alsu Akhmetshina
Chemistry



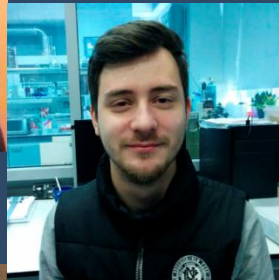
Nail Yanbikov
Chemical Technology



Artem Atlaskin
Chemical Technology



Stanislav Battalov
Chemical Technology



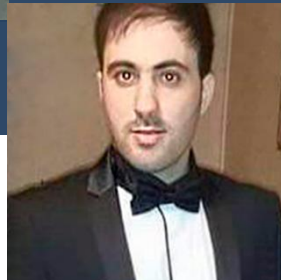
Egor Puzanov
Chemical Technology



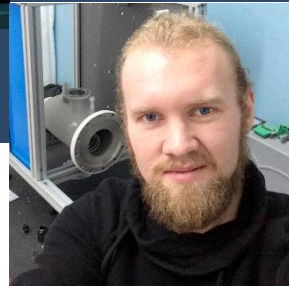
Kseniya Otvagina
Chemistry



Amal Mechergui
Chemistry



Amin Kassau
Chemical Technology



Nikolai Uglov
Chemical Technology





MATERIAL SCIENCE



NEW MEMBRANE MATERIALS
(Polymeric and ceramic)



HYBRID MEMBRANES
(MMM, SLIMS, POLYRTILS)

CHEMICAL ENGINEERING



INTENSIFICATION OF MEMBRANE PROCESSES
(Cascades, new module)



HYBRID PROCESSES
(Membrane contactors,
Membrane Absorption)



APPLICATIONS OF MEMBRANE GAS SEPARATION

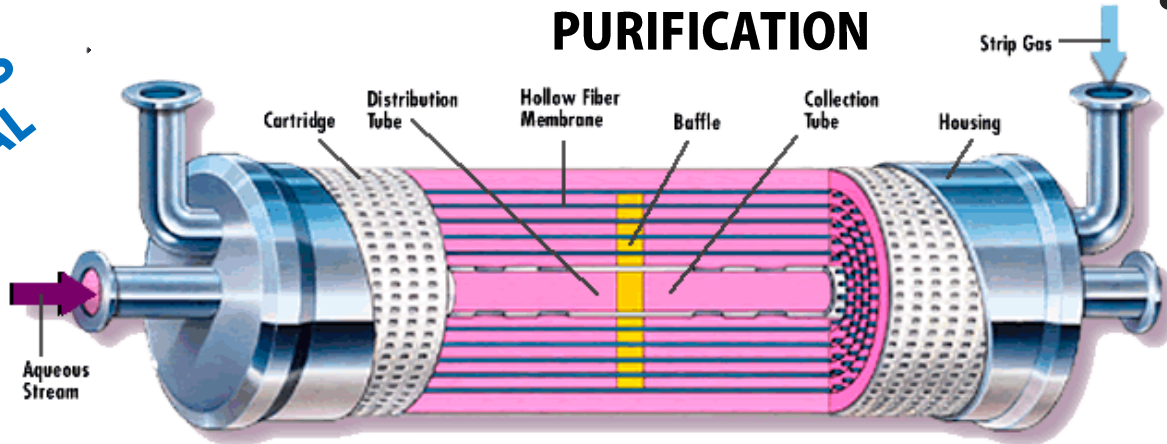
HYSEP[®]
Hydrogen Separation Modules

99.999999

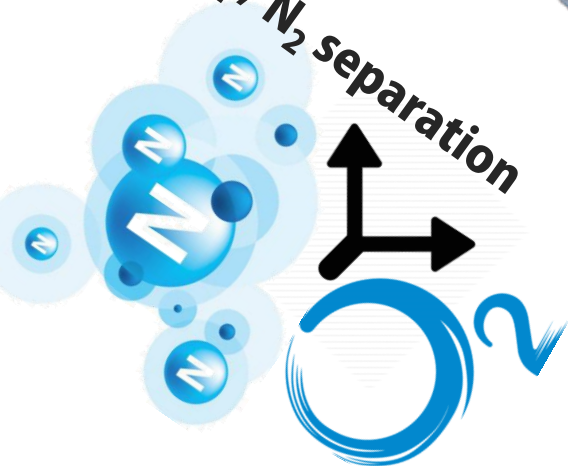
GASES HIGH PURIFICATION



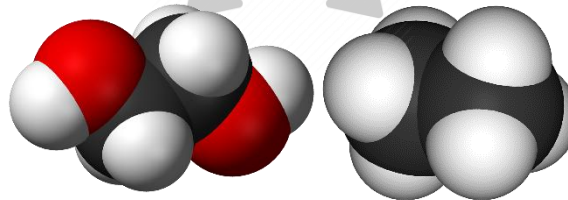
ACID GASES REMOVAL



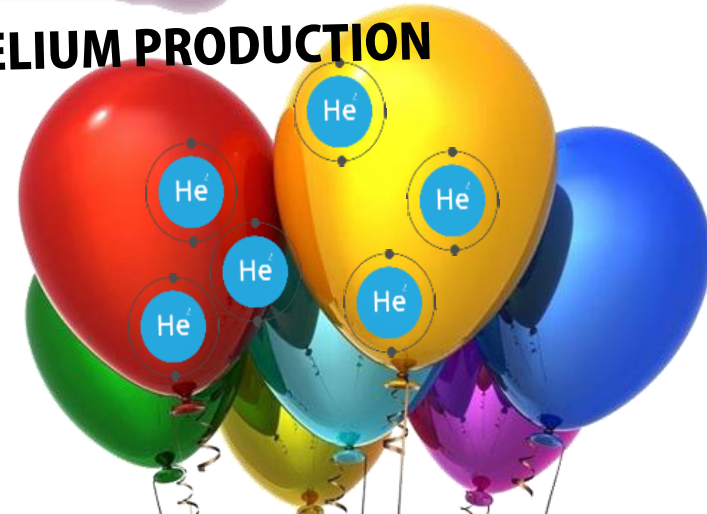
O₂ / N₂ separation

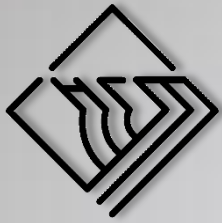


Olefin/Paraffin separation



HELIUM PRODUCTION





OUR SEPARATION AND PURIFICATION TECHNOLOGIES

99.9999%
 AsH_3 , SiH_4 , GeH_4 , NH_3 , PH_3 , N_2O , PH_3

SEPARATION AND PURIFICATION GASES

CH₄, CO₂, CH₄/He
 natural gas and biogas treatment
 CO₂ CAPTURE
 olefin / paraffin

engineering optimization intensification

cost reduction

hybridization energy efficiency

Separation and Purification Technology
 Volume 135, 15 October 2014, Pages 117-126

High-pressure distillation: Simultaneous impact of pressure, temperature and loading on separation performance during distillation of high-purity gases in high-performance randomly-packed columns

Maxim M. Trubyanov^a, Georgiy M. Mochalov^a, Vladimir M. Vorotyntsev^a, Sergey S. Suvorov^a
^a Department of Nanotechnology and Biotechnology, Institute of Physicochemical Technologies and Material Science, Nizhny Novgorod State Technical University n.a. R.E. Alexeev, 24 Minina Str., 603950 Nizhny Novgorod, Russian Federation

Separation of ammonia-containing gas mixtures in a one-compressor multistage membrane apparatus

Authors: I.V. Vorotyntsev, D.N. Shalykin, P.N. Drozdov, M.M. Trubyanov, A.N. Petukhov, S.V. Batalov

Journal: *Journal of Membrane Science*, February 2017, Volume 531, Issue 2, pp 517-531

Unsteady-state membrane gas separation by novel pulsed retentate mode for improved membrane module performance: Modelling and experimental verification

Journal: *Journal of Membrane Science*, Volume 530, 15 May 2017, Pages 53-64

Authors: Maxim M. Trubyanov, Pavel N. Drozdov, Artem A. Afanasyev, Stanislav V. Batalov, Igor S. Puzanov, Andrey V. Vorotyntsev, Anton N. Petukhov, Vladimir M. Vorotyntsev, Ilya V. Vorotyntsev

Desalination and Water Treatment
 www.deswater.com

Towards the potential of absorbing pervaporation based on ionic liquids for gas mixture separation

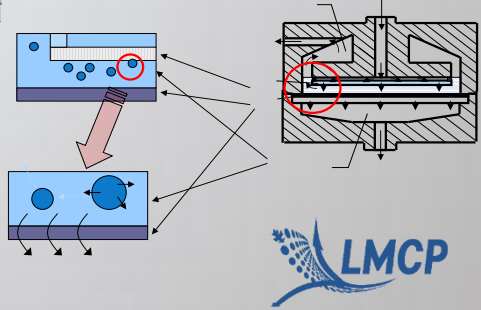
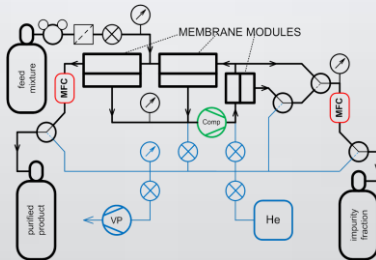
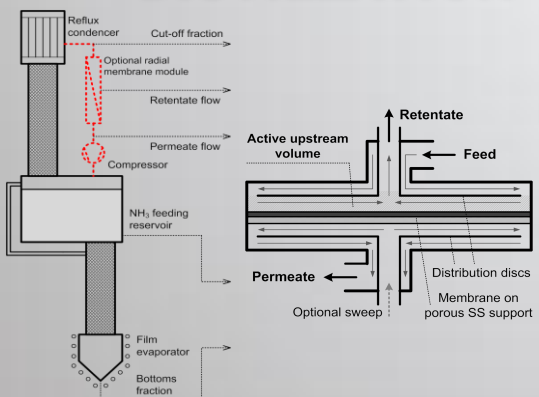
Ilya V. Vorotyntsev^a, Artem A. Afanasyev^a, Maxim M. Trubyanov^a, Anton N. Petukhov^a, Olesya R. Guseynova^a, Alsu I. Akhmetshina^a, Vladimir M. Vorotyntsev^a

HYBRIDIZATION

Elevated pressure DISTILLATION

MEMBRANE gas separation

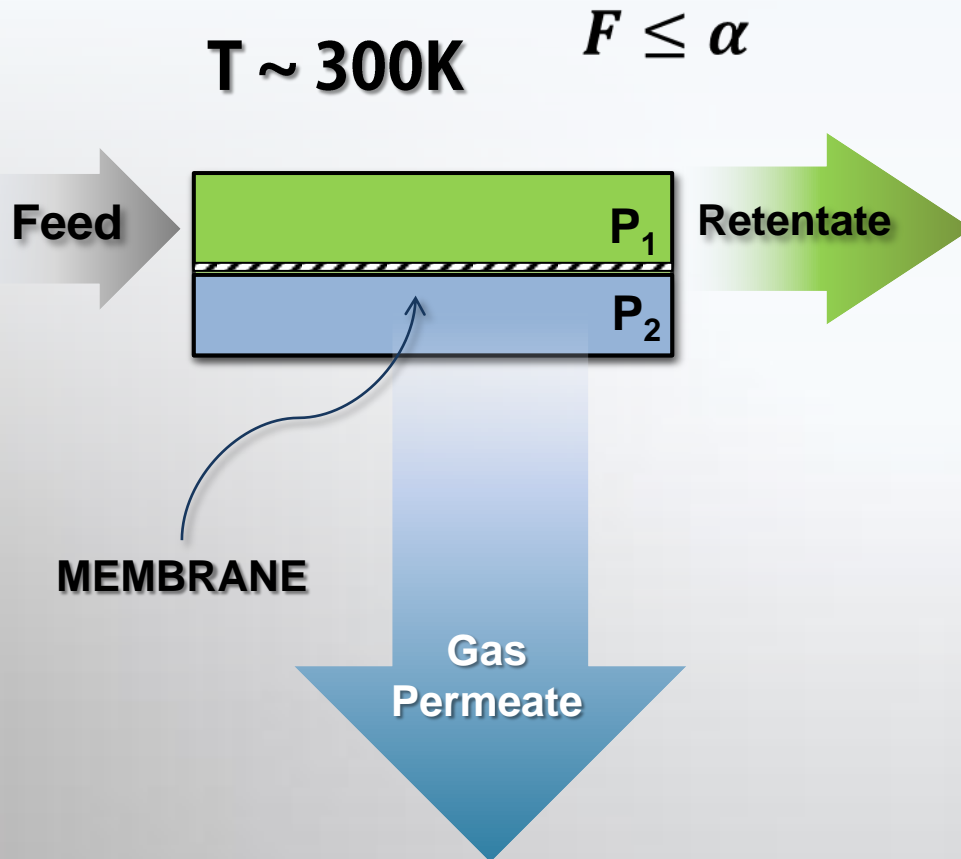
Absorbing PERVAPORATION





SCHEME OF MEMBRANE GAS SEPARATION MODULE AND RECTIFICATION COLUMN

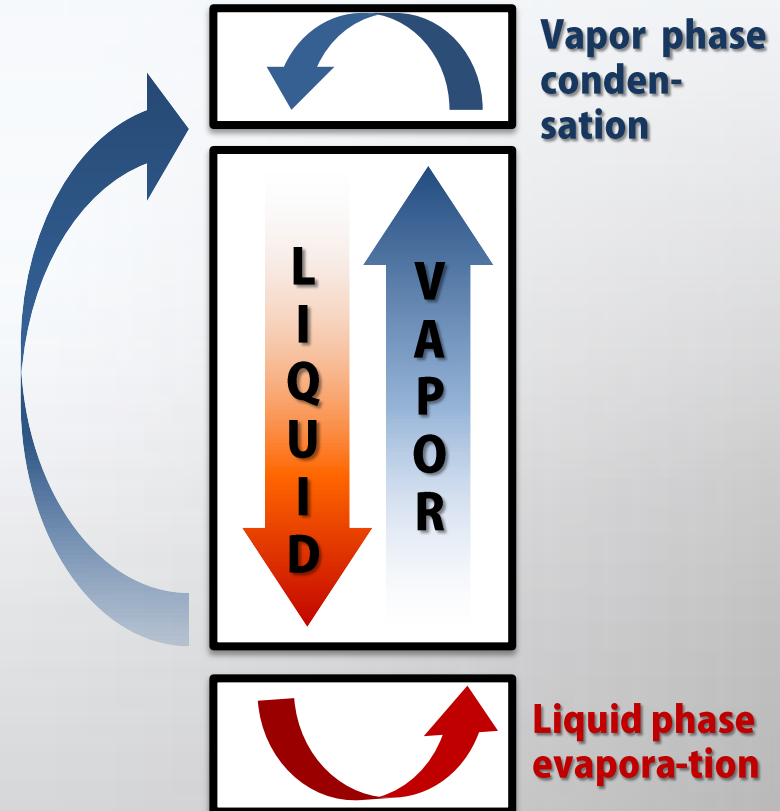
SINGLE-STAGE PROCESS
DIRECT CURRENT FLOW PROCESS



MULTI-STAGE PROCESS
COUNTER CURRENT FLOW PROCESS

$$F = \alpha_{l-v}^n \quad T = T_{b.p.} \ll 300K$$

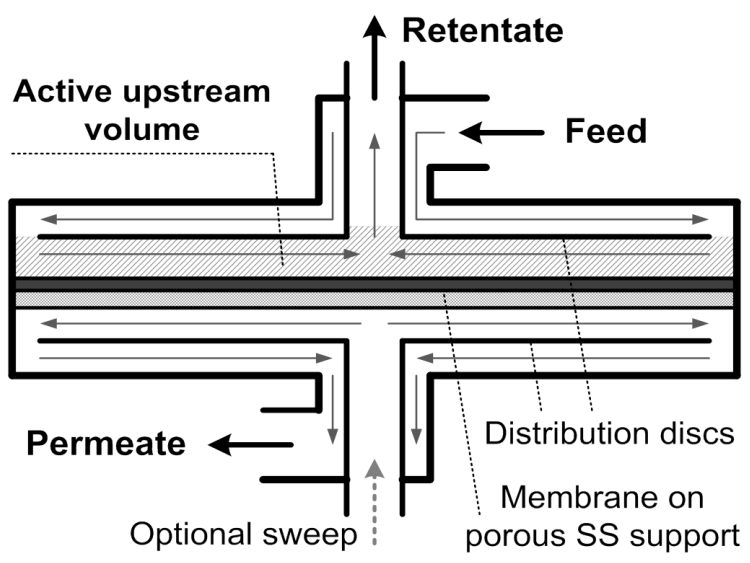
n – the number of separation stages.



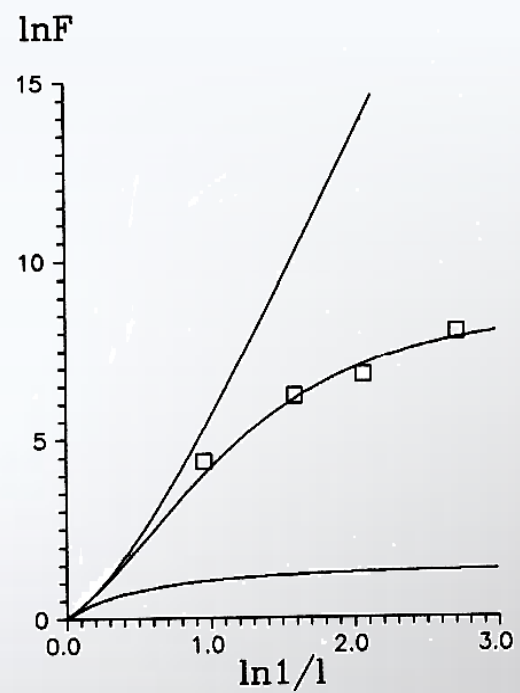
CHARACTERISTICS OF THE MEMBRANE MODULE



THE RADIAL COUNTERCURRENT MEMBRANE MODULE:



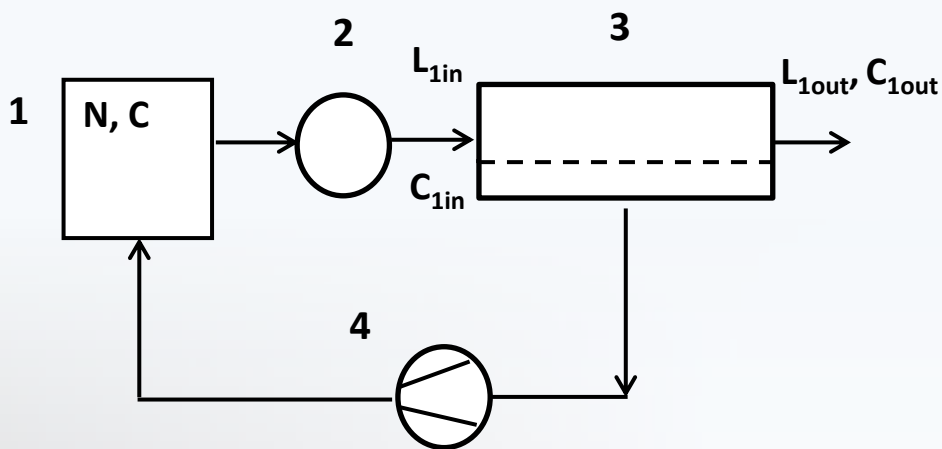
THE DEPENDENCE OF THE SEPARATION FACTOR F OF THE DEGREE OF SEPARATION MONOGERMANE (GeH_4) FROM WATER (H_2O)



- 1 – calculation according to the model of ideal displacement;
- 2 – calculation according to the model of complete mixing;
- 3 – experimental data



CASCADE OF MEMBRANE MODULE WITH FEEDING RESERVOIR (FD)

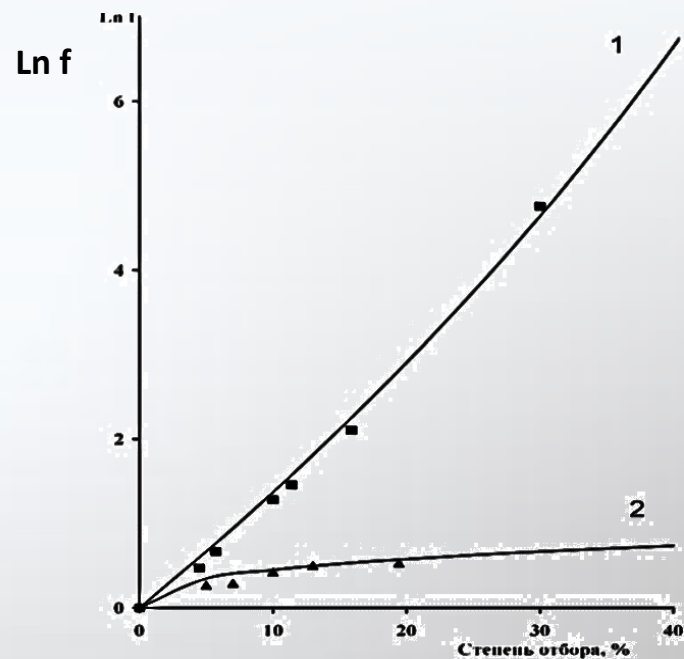


1 – feeding reservoir (FD); 2 – pressure reducer; 3 – membrane module; 4 – vacuum-compressor

$$f = \frac{C_0}{C} = \left(\frac{N_0}{N} \right)^{F^{-1}-1}$$

N_0 – quantity mole of the mixture in a FD at initial time,
 N - quantity mole of the mixture in a FD after purification

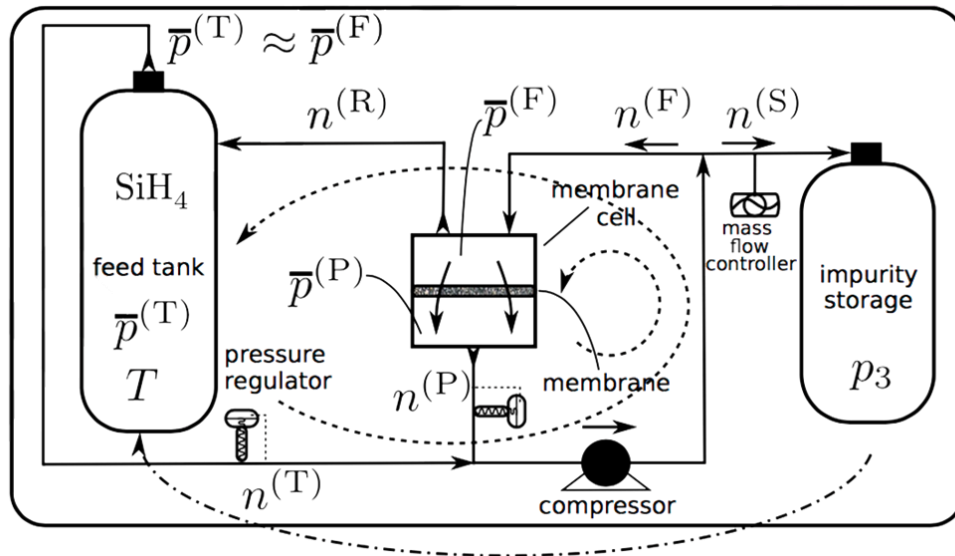
THE DEPENDENCE OF PURIFICATION RATIO FROM QUANTITY OF SAMPLED SUBSTANCES MIXTURE: R-12 (CF_2CL_2) – IMPURITY OF R-218 (C_3F_8)= 2.94



Quantity of picked gas, %

1 – membrane module with a feeding reservoir;
 2 – single membrane module

FAST-PERMEANT IMPURITY DEPLETION LOOP



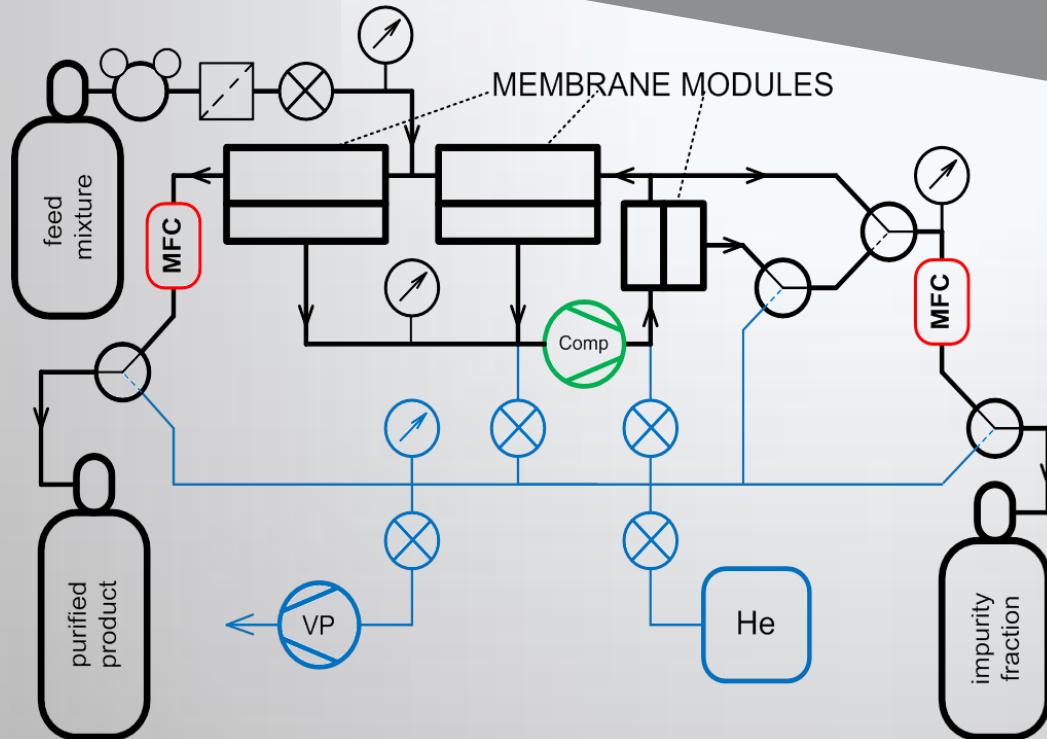
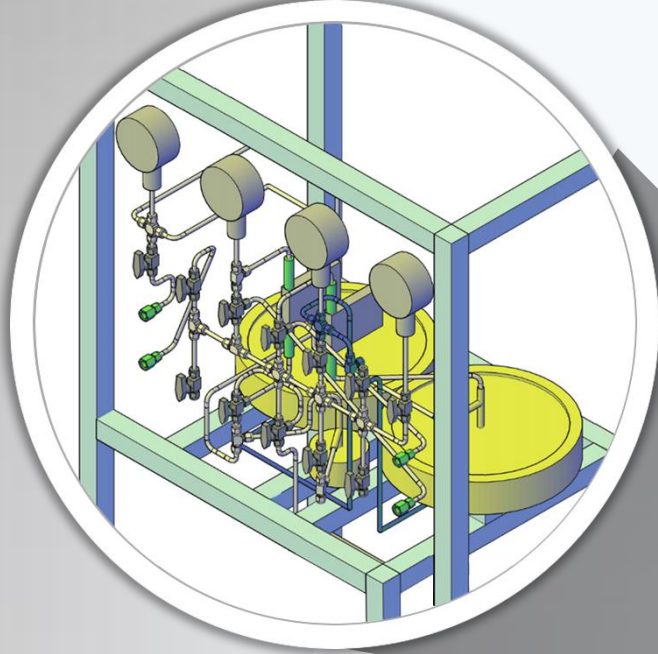
The silane product is concentrated in the feed tank via recirculation of the retentate, and the impurity is concentrated on the smaller loop which discharges to the impurity storage. The impurity can be recycled as feed (dashed – dotted line).



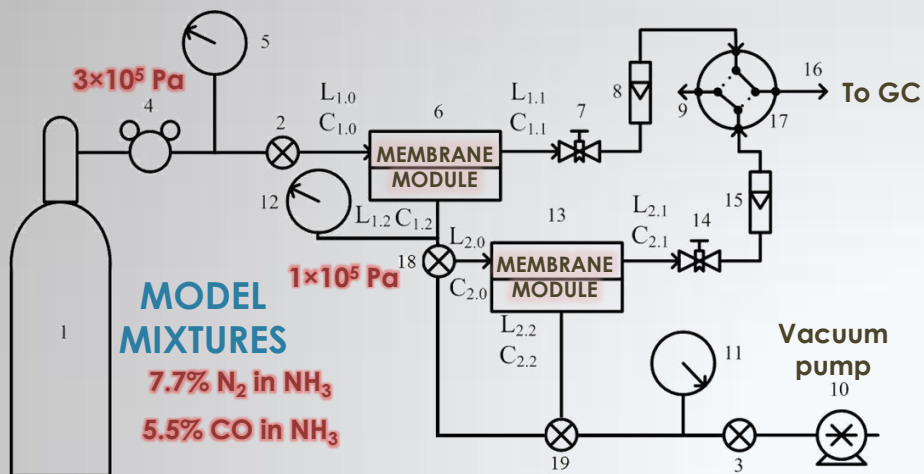
EXPERIMENTAL SLOW-PERMEANT IMPURITY DEPLETION LOOP CURRENTLY IN TESTING

doi.org/10.1016/j.memsci.2016.12.049

MEMBRANE CASCADE TYPE OF «CONTINUOUS MEMBRANE COLUMN»



ONE-COMPRESSOR ONE-TWO-STAGE MEMBRANE APPARATUS FOR AMMONIA-BASED MIXTURES SEPARATION



SEPARATION FACTOR:

$$F^{-1} = \frac{C_{1,1}}{C_{1,0}} = \left(\frac{L_{1,0}}{L_{1,1}} \right)^{(\alpha^* - 1)/\alpha^*} \quad \text{ideal mixing regime}$$

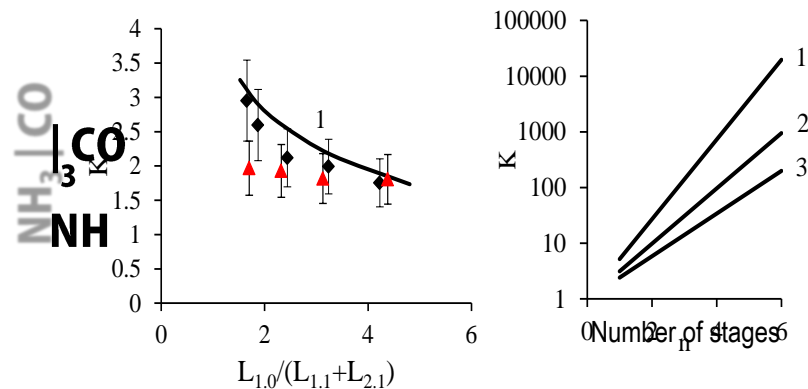
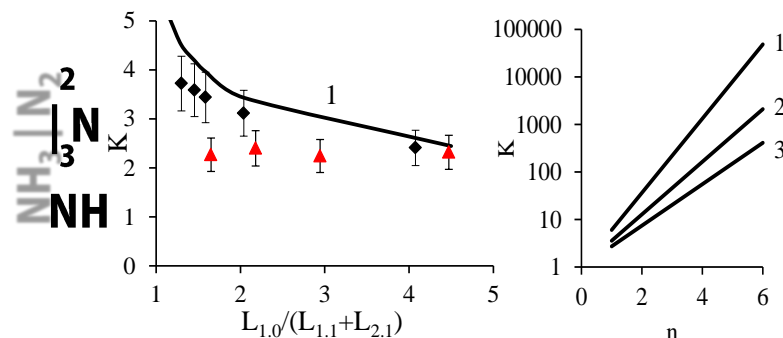
PURIFICATION DEGREE:

$$K = \frac{C_{1,0}}{C_{1,2}}$$

$$K_{1-n} = c_{1,0} / c_{n,2} = \left[\frac{\Theta}{1 - (1 - \Theta) F_i^{-1}} \right]^n = \left[\frac{\Theta}{1 - (1 - \Theta) \frac{1}{\alpha_i^*}} \right]^n$$

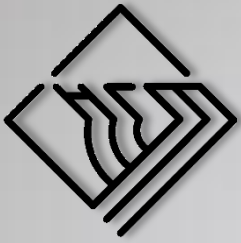
ONE-COMPRESSOR MULTISTAGE MEMBRANE APPARATUS

PURIFICATION DEGREE



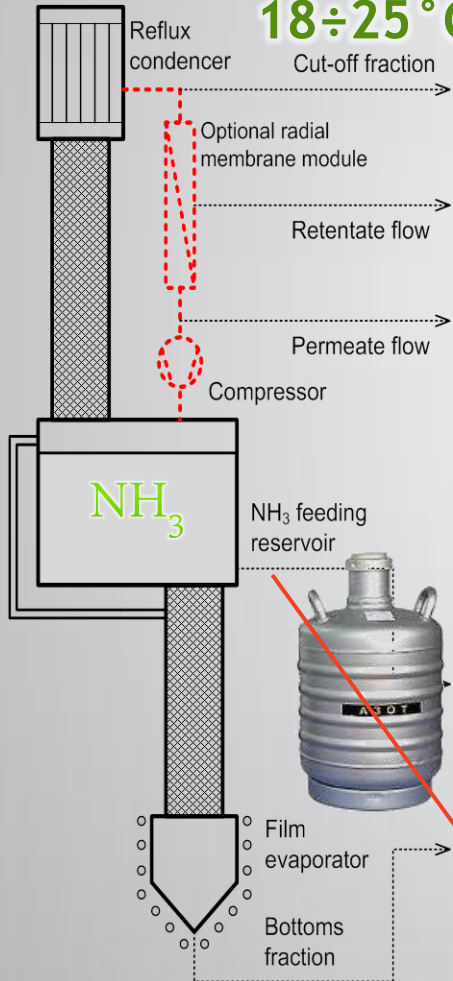
SAMPLING RATIO:

1 – 70%; 2 – 15%; 3 – 5%.
 ▲ – one stage of the cascade
 ◆ – two stages of the cascade

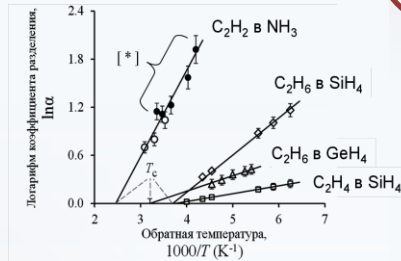


MEMBRANE SEPARATION + DISTILLATION UNDER ELEVATED PRESSURE

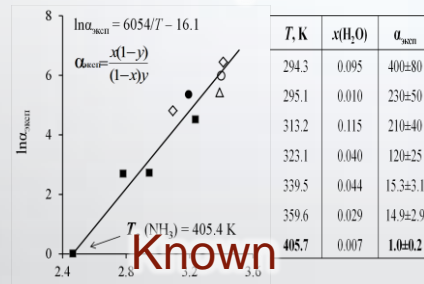
8 ÷ 12 atm
18 ÷ 25 °C



Decrease
in liquid-vapor
distribution coefficient

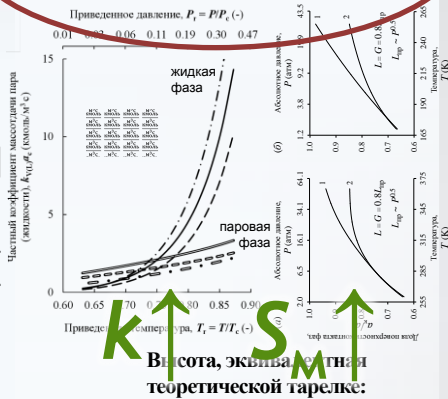


Примесь	α (239.8 K)	α (293 K)	A	$B \times 10^{-3}$
C ₂ H ₂	6.3 ± 1.8	2.7 ± 0.8	-2.67	1.08
N ₂ (H ₂)	(2.8 ± 0.2) × 10 ⁴	920 ± 80	-8.27	4.44
C ₃ H ₆	100 ± 10	12.2 ± 0.9	-6.67	2.7
C ₃ H ₈	490 ± 60	29 ± 5	-8.98	3.64
CH ₃ OH	27.2 ± 2.2	-8.84		
H ₂ O	(7.1 ± 0.5) × 10 ⁴	100 ± 80	-16.1	6.4

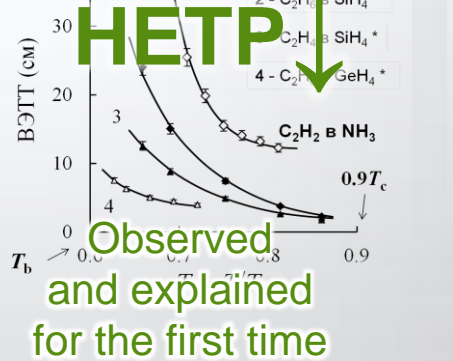


Known
previously

MASS-TRANSFER INTENSIFICATION

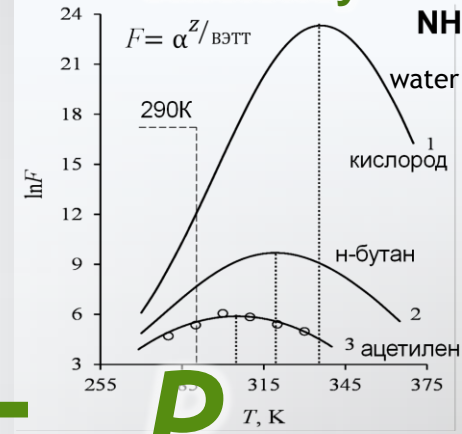


$$k \uparrow, S_M \uparrow \Rightarrow \text{Высота, эквивалентная теоретической тарелке:}$$



Observed
and explained
for the first time

OPTIMAL P & T for maximum efficiency



АЛГОРИТМ РАСЧЕТА ФАКТОРА ЭФФЕКТИВНОСТИ КОЛОННЫ В СТАЦИОНАРНОМ РЕЖИМЕ

термодинамический фактор $F = \frac{\alpha_{\text{верх}}}{\alpha_{\text{низ}}} = \frac{\alpha^Z}{\text{ВЭТТ}}$

кинетический фактор $F = f(P, T, L)$

$\ln \alpha_{\text{эксп}} = A + BT^{-1}$

$\ln \alpha_{\text{эксп}} = \frac{x(1-y)}{(1-x)y}$

$\text{ВЭТТ} = \frac{\ln \alpha}{\alpha - 1} \left(\frac{U_y}{k_y a_k} + \frac{U_x}{k_x a_k} \right)$

параметры массопереноса: $\frac{D_{12}}{a_k} = f \left(\frac{D_{12}}{a_k} \right) = f \left(\frac{D_{12}}{a_k} \right) = f \left(\frac{D_{12}}{a_k} \right)$

скорости в фазе: $U_i = \frac{L_i}{P_i} \quad U_i = \frac{G_i}{P_i}$

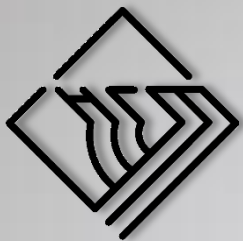
пример для СН частные коэффициенты вымосточены в фазе, поверхность в контакт с фазой: $1/k_x = (a_k^{1/2} D_{12}^{-1/2}) (D_{12}^{1/2} / 0.0218 a_k) (a_k / 140)^{1/2}$; $1/k_y = (a_k^{1/2} D_{12}^{-1/2}) (D_{12}^{1/2} / 0.118 a_k) (a_k / 140)^{1/2}$; $a_k = 0.04$

близкие коэффициенты диффузии в жидкой и паровой фазах, удельные газ-жидкостные коэффициенты на основе a_k в таблице жидкой фазы.

$D_{12} = 1.85 \times 10^{-5} \text{ м}^2/\text{с}$; $U_{\text{ж}} = 0.01 \text{ м}^3/\text{с}$; $U_{\text{п}} = 0.01 \text{ м}^3/\text{с}$; $H_{\text{ж}} = 1 \text{ м}$; $H_{\text{п}} = 1 \text{ м}$; $a_k = 0.04$; $a_k = 0.04$...

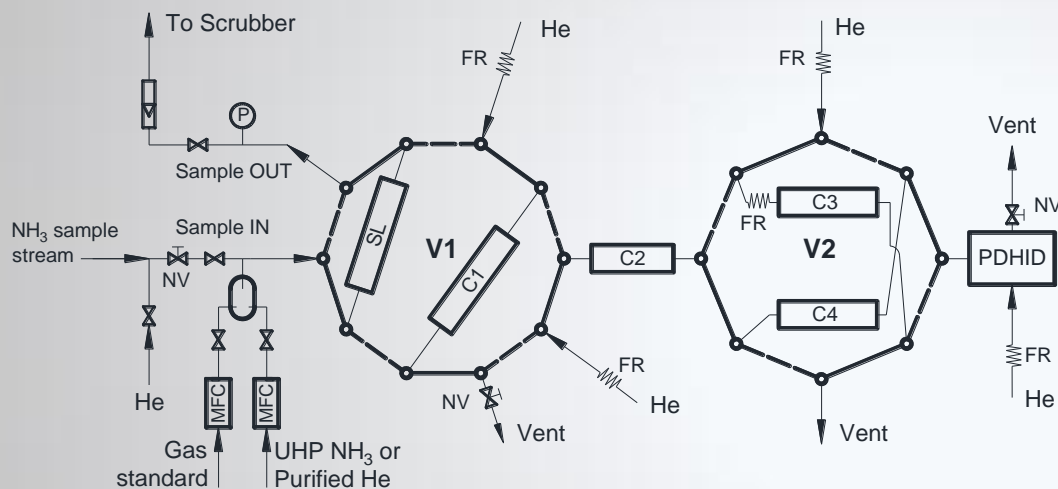
факторы: $\text{ВЭТТ} = \frac{L}{P} \quad \text{ВЭТТ} = \frac{G}{P}$

KNOW HOW

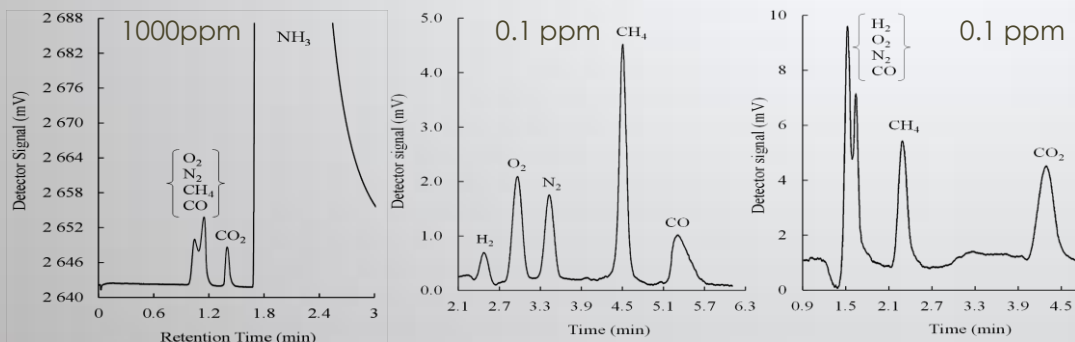


MEMBRANE SEPARATION + DISTILLATION UNDER ELEVATED PRESSURE

Two-dimensional GC-PDHID|TCD analytical system for [sub-ppm ÷ 100%] determination of H₂, O₂, N₂, CH₄, CO, CO₂



Chromatograms of impurities in ammonia



Component of the GC-system	Characteristics
Detector	PDHID D-2-I, 100°C
First column to separate the ammonia matrix, C1	15% PEG-600 on PTFE, 70°C 60/80 mesh 3 m × 3 mm i.d.
Analytical column, C3 (for H₂, O₂, N₂, CH₄, CO)	13X molecular sieve, 70°C 60/80 mesh 1 m × 2 mm i.d.
Analytical column, C4 (for CO₂)	Porapak Q, 70°C 60/80 mesh 4 m × 2 mm i.d.
Trace ammonia trap, C2	NaHSO ₄ , 70°C 40/60 mesh 0.3 m × 3 mm i.d.
Sample loop, SL	1.5 ml, 70°C
Carrier gas, He	He 99.99999+%, 30 ml/min

ANALYTICAL CONTROL OF THE PURIFICATION PROCESS. FTIR

GAS CELL - 22m
PIKE (USA)

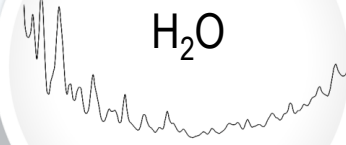
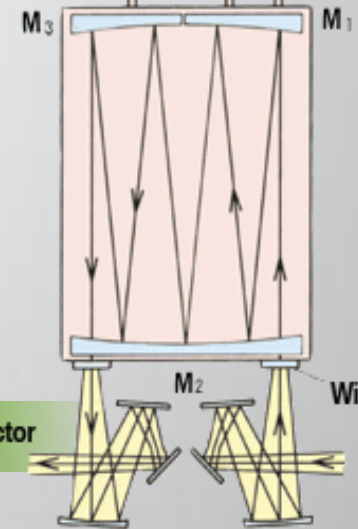
FTIR
Shimadzu IRAffinity-1
(Japan)

RECORDLY LOW LIMITS OF DETECTION

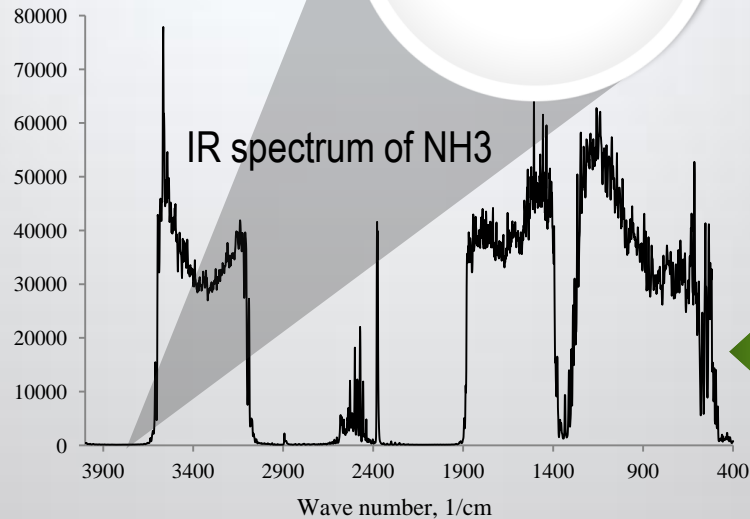
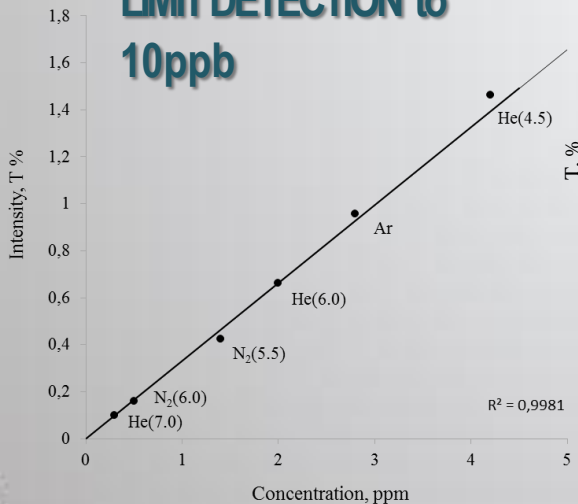
100% - 10⁻⁷%!

H₂O + NH₃
inlet/outlet
pipes

Pressure gauge



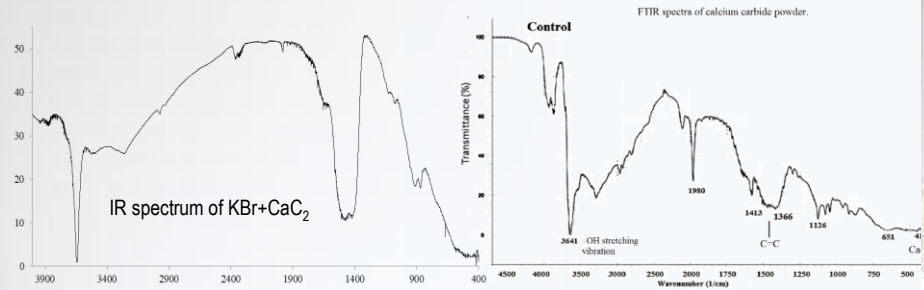
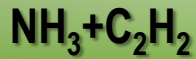
LIMIT DETECTION to
10ppb





ANALYTICAL CONTROL OF THE PURIFICATION PROCESS. GAS CHROMATOGRAPHY

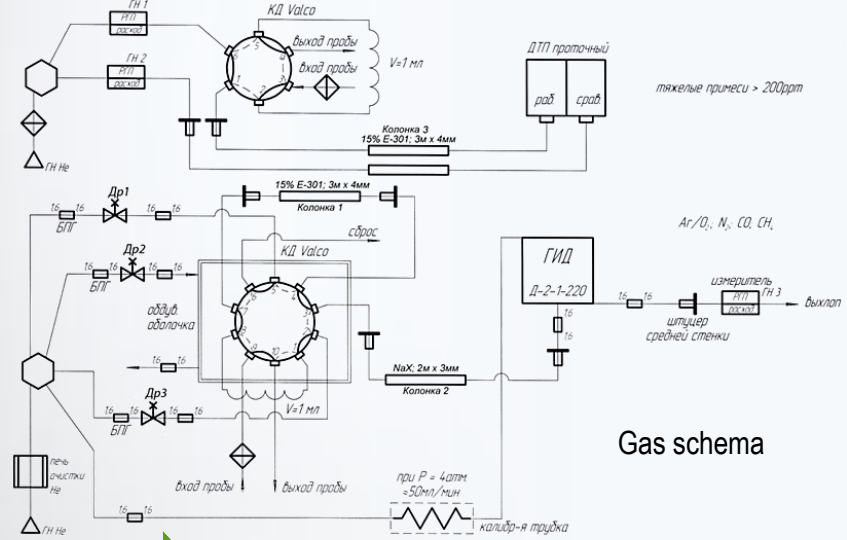
CaC₂ reactor



Planetary ball mill PM100 Retsch (USA)

LIMIT DETECTION
100% - 10⁻⁴ %

Mr. Trivedi. Effect of Biofield Energy Treatment on Physical and Structural Properties of Calcium Carbide and Praseodymium Oxide



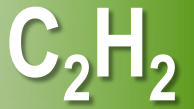
Gas schema



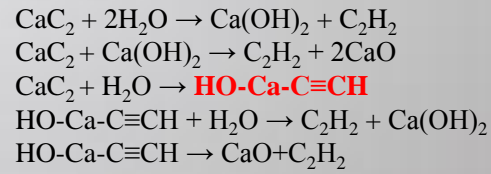
CaC₂



XROMOC GX-1000 (RUSSIA) + PDHID (Valco VICI, USA)



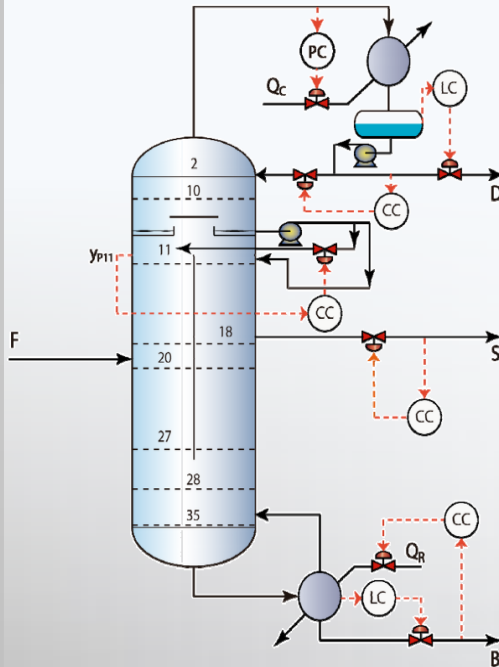
CONCENTRATIONS
 $\text{C}_2\text{H}_2 \sim \text{H}_2\text{O}$



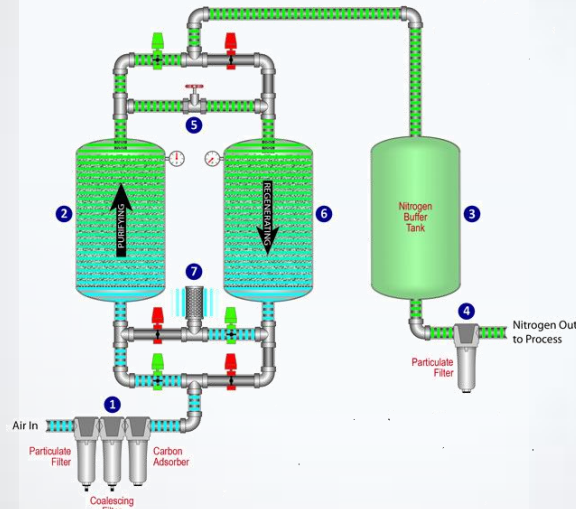


EXAMPLES OF UNSTEADY-STATE PERIODICAL SEPARATION TECHNIQUES

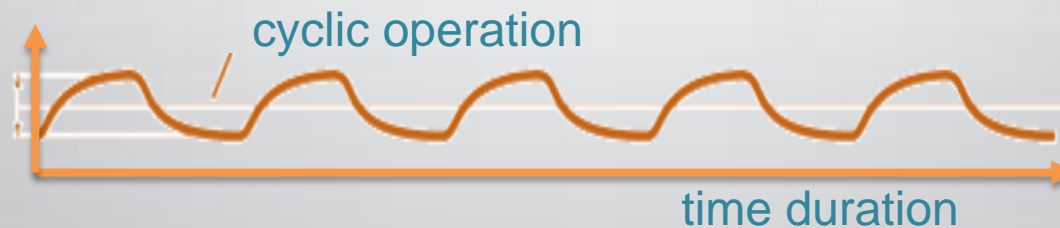
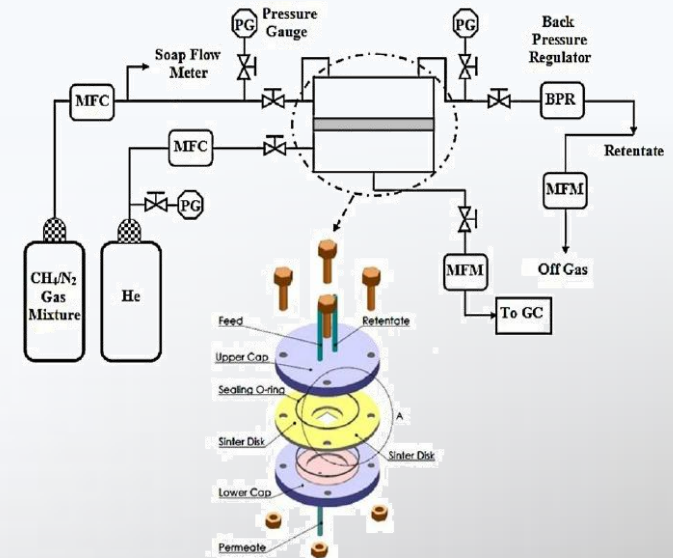
DISTILLATION



PRESSURE SWING ABSORPTION



MEMBRANE SEPARATION





BATCH DISTILLATION WITH PERIODICAL WITHDRAWALS

Kinetics of concentrating and ultrapurifying dichlorosilane by batch distillation with periodical withdrawals

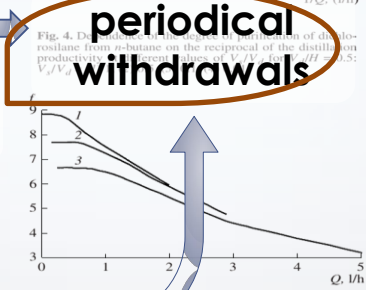
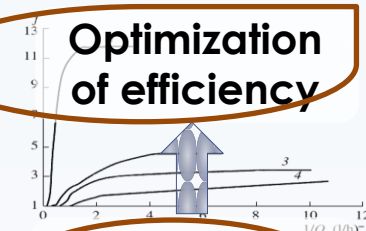
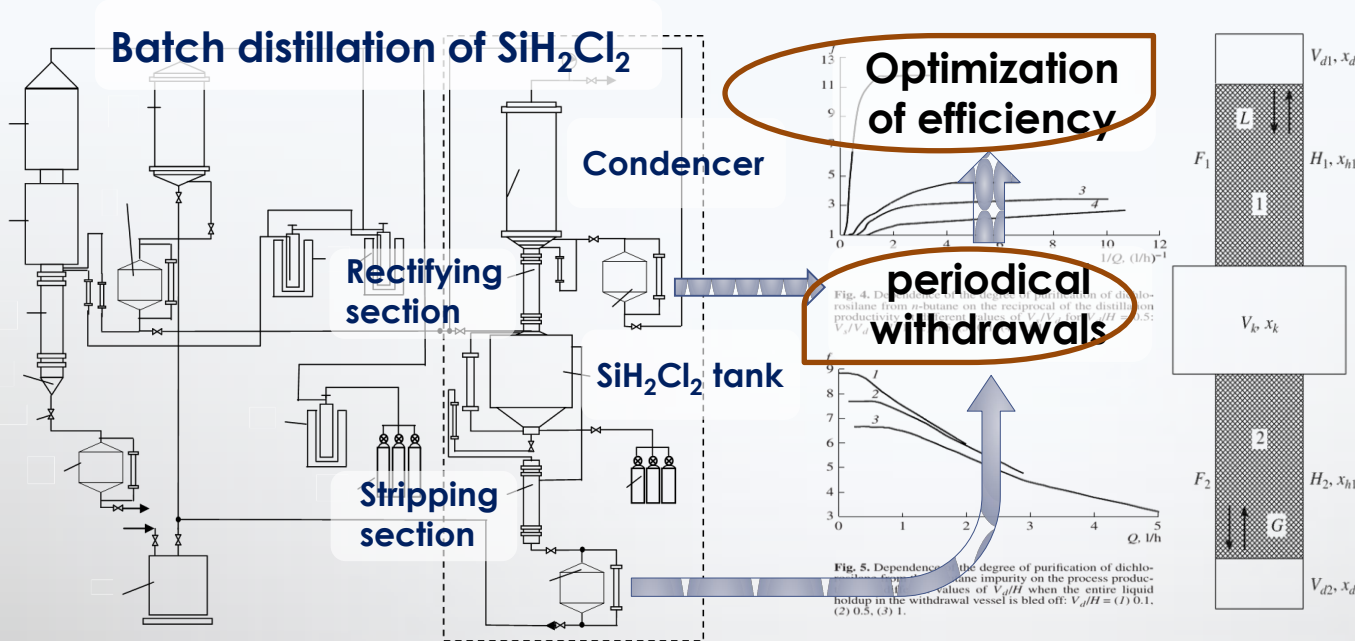
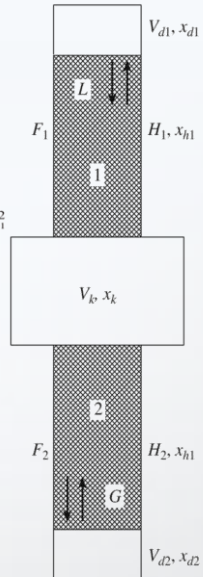


Fig. 4. Dependence of the degree of purification of dichlorosilane from isobutane on the reciprocal of the distillation productivity for different values of V_d/H and V_s/H : (1) 0.5; (2) 0.5, (3) 1.

Fig. 5. Dependence of the degree of purification of dichlorosilane impurity on the process productivity for different values of V_d/H when the entire liquid holdup in the withdrawal vessel is bled off: $V_d/H = (1) 0.1$; (2) 0.5, (3) 1.



Current and disturbed Separation Factors

$$F_{1,2} = \frac{x_{d1,2}(1-x_k)}{(1-x_{d1,2})x_k} \quad \tilde{F}_{1(2)} = \frac{H_{1(2)} - V_{s1(2)}}{H_{1(2)}}$$

Relaxation time for the disturbed separation factor

$$t = \alpha \frac{[V_d(F_0 - 1) + \left(\frac{F_0 - 1}{\ln F_0} - 1\right)H]}{L(\alpha - 1)} \ln \frac{F_0 - 1}{F_0 - F}$$



UNSTEADY-STATE MEMBRANE GAS SEPARATION BY CONCENTRATION PULSE

PULSED INPUT OF THE FEED MIXTURE

Separated mixture
 $\text{He} : \text{CO}_2 = 1 : 1$

Membrane
PVTMS

Equal permeability

$P_{\text{He}} \approx P_{\text{CO}_2}$

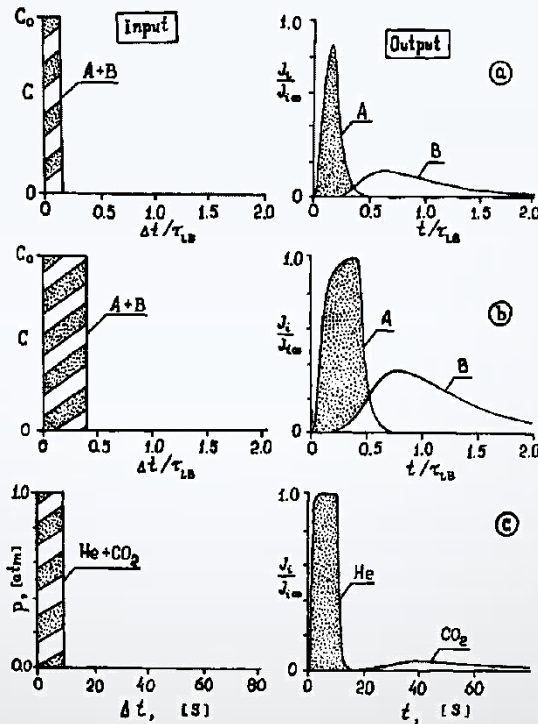


Different diffusivity

$D_{\text{He}} \approx 47 D_{\text{CO}_2}$

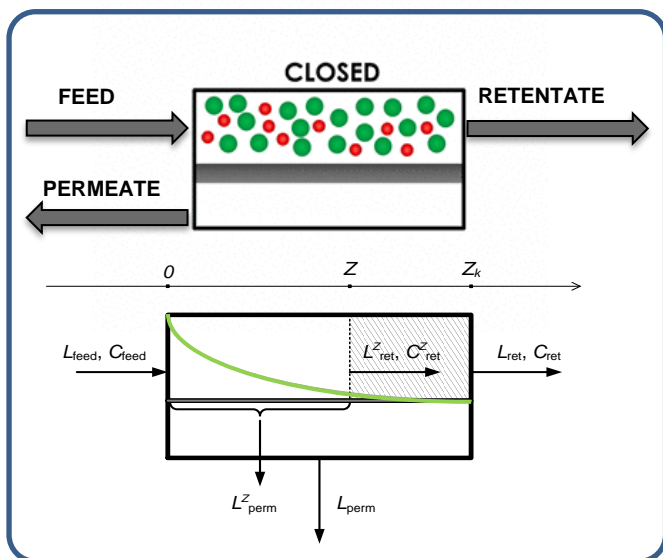


PULSED INPUT



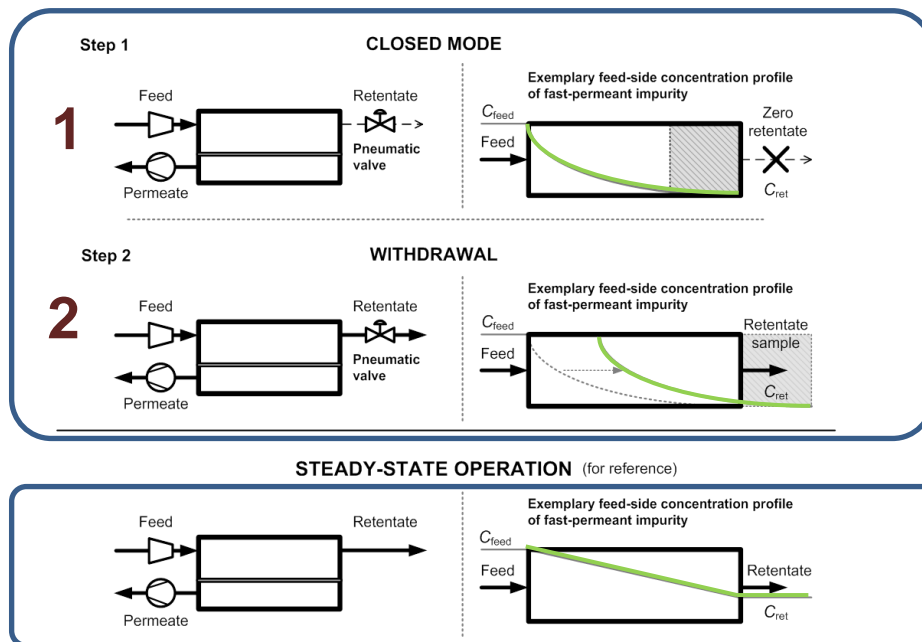
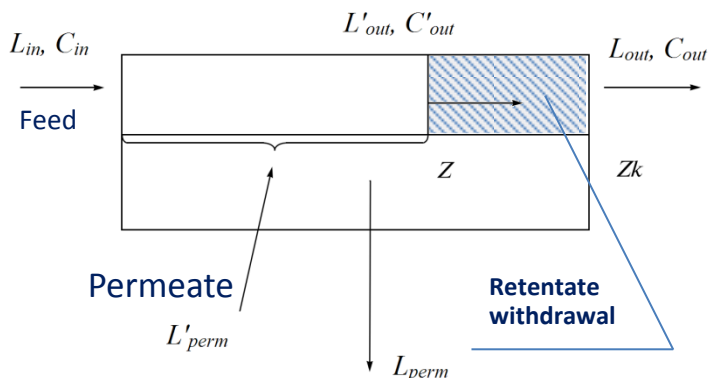
- Separation on non-selective membrane
- Increase in selectivity for **diffusion-controlled** separation
- **Decrease in productivity**

Working principle of Pulsed retentate operation



Removal of highly penetrating impurity

Theoretical modeling



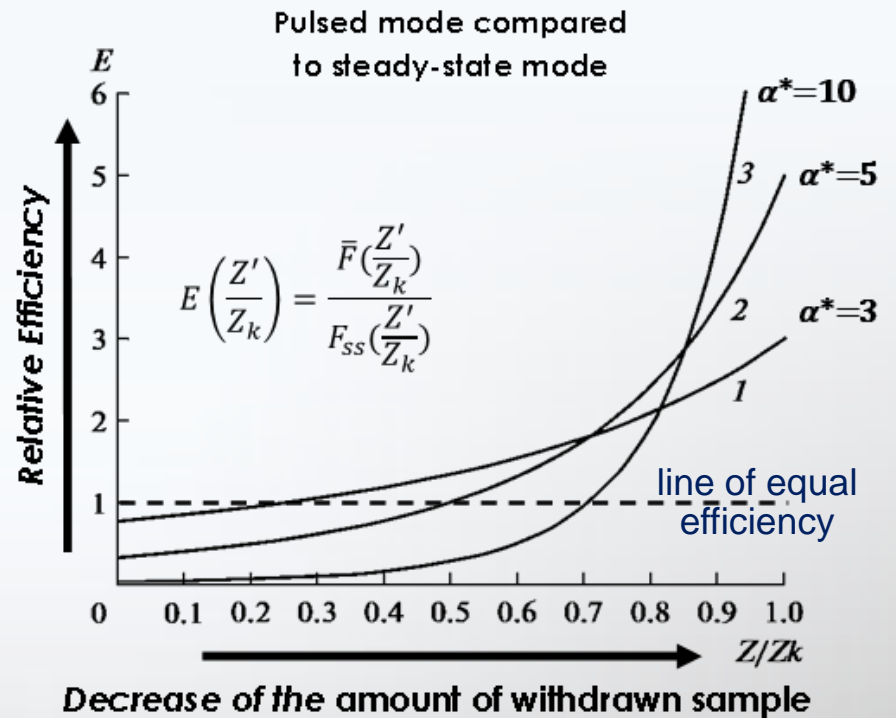
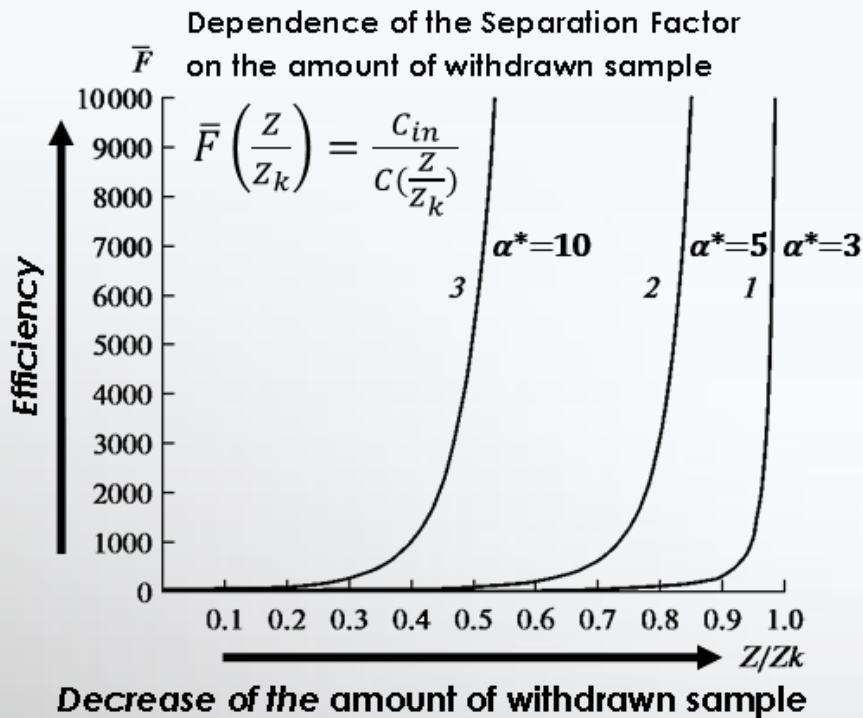
Separation factor (pulsed mode)

$$F' = \frac{C_{in}}{C'_{out}} = \left(\frac{L_{in}}{L'_{out}}\right)^{\alpha^* - 1}$$

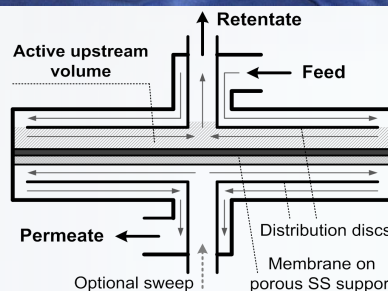
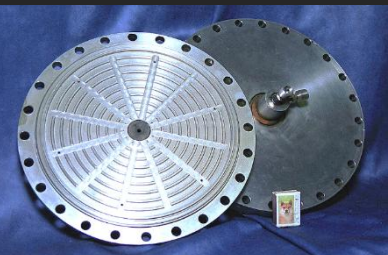
$$\alpha^* = \frac{\alpha}{1 + (\alpha - 1) \frac{P_2}{P_1}}$$

C_{in}/C'_{out} - inlet and outlet concentrations ratio; L_{in} , L_{out} , L_{perm} - inlet, outlet, permeate fluxes; α - ideal selectivity; α^* - effective selectivity; P_2 and P_1 - permeate and feed pressure

Efficiency vs productivity compared to steady-state



EXPERIMENTAL SETUP FOR UNSTEADY-STATE MEMBRANE GAS SEPARATION



SYSTEM DESCRIPTION

Membrane
Poly(arylate-siloxane) Silar®

Gas mixture
 $N_2 : N_2O = 1 : 0.01$
 $\alpha_{ideal}(N_2O / N_2) = 12.0 \pm 0.7$

Operational parameters

- Stage cut
- Pressure ratio
- $\Delta\tau_{open}$ – duration of withdrawal
- $\Delta\tau_{close}$ – duration of stripping
- $\Delta\tau_{total}$ – total cycle duration
- Sample amount ratio

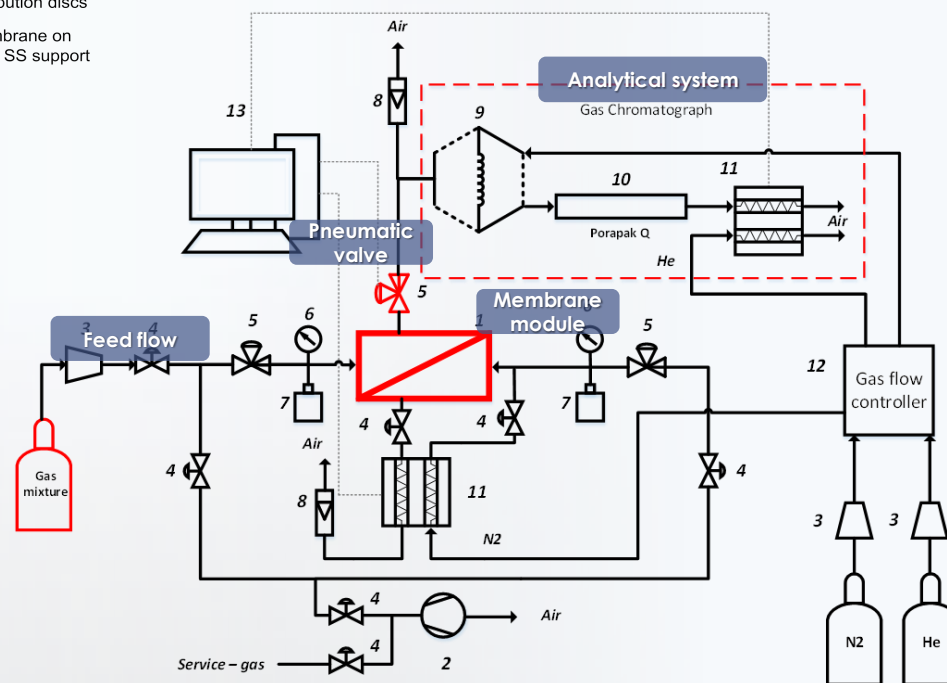
Nitrogen-based model mixtures and GC conditions

Gas	Q (Barer)	α_{id}	α_{ef}
N ₂	200±5	-	-
CH ₄	550±15	2.75±0.15	2.7±0.5
CO ₂	1800±50	9.0±0.5	7.5±1.5
N ₂ O	2400±70	12.0±0.7	10±2
Component of the GC		Characteristics	
Detector	TCD, 100mA, 100°C		
Chromatographic column	Porapak Q, 60/80 mesh, 80°C 2 m × 3 mm i.d. stainless steel tube		
Sample loop	3 ml, 80°C		
Carrier gas	He 99.9999%, 30 ml/min		

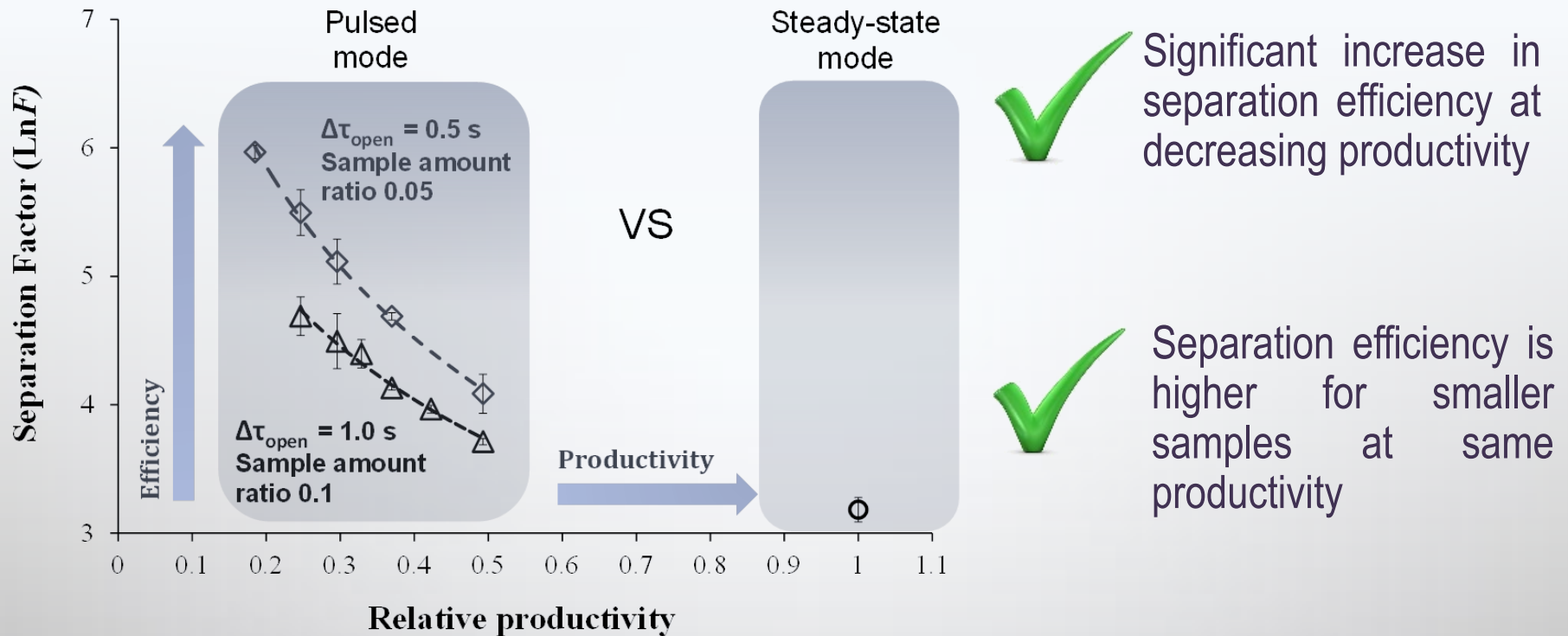
High-efficient radial membrane module in counter-current mode:



low variation of the gas linear velocity helps to provide the laminar gas flow eliminates any trapped gas or dead zones

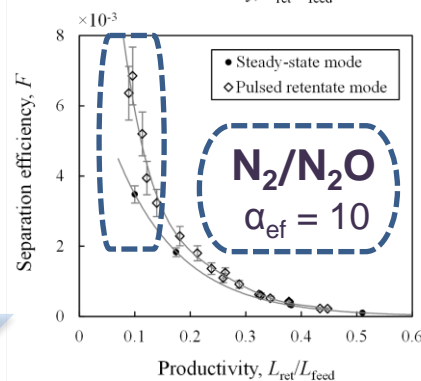
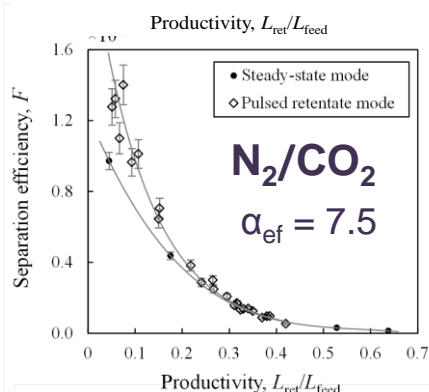
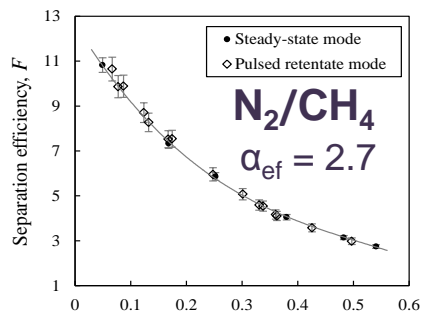


COMPARISON OF A PULSED MODE AND A STEADY-STATE MODE



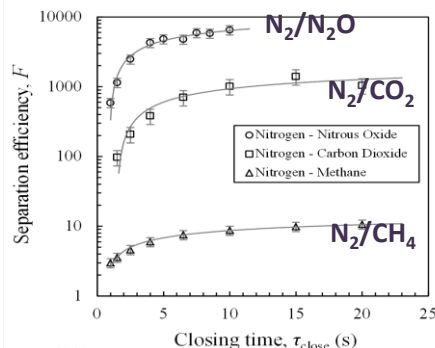
DETAILED EXPERIMENTAL VERIFICATION

SEPARATION OF BINARY MIXTURES IN RADIAL COUNTERCURRENT MEMBRANE MODULE IN TWO REGIMES

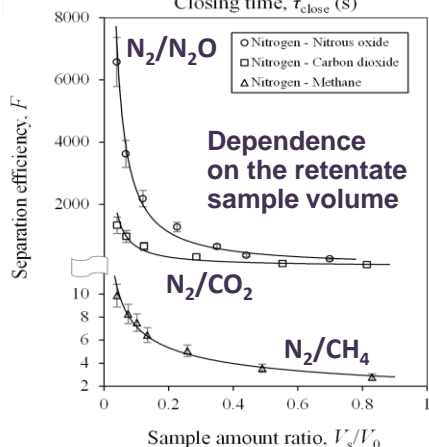


The higher the selectivity the higher the efficiency improvement

APPROACHING CLOSED MODE OPERATION



Time period to reach a steady-state condition of a closed mode; opening time is 0.5 s for each data point.

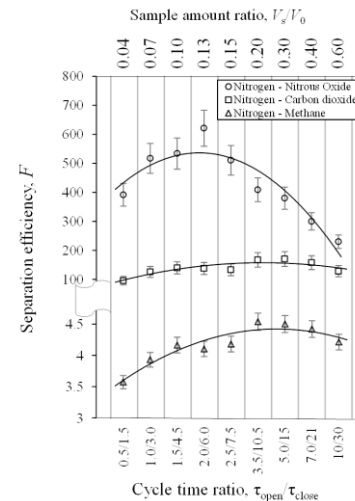


Separation performance depending on retentate sample amount ratio (V_s volume of retentate sample, and V_0 active upstream volume).

Remarks

- Separation efficiency increases with the increase of stripping time
- With the increase of stripping time the system approaches closed mode operation
- Smallest retentate sample volume provides the highest separation efficiency

OPTIMIZATION PERSPECTIVES

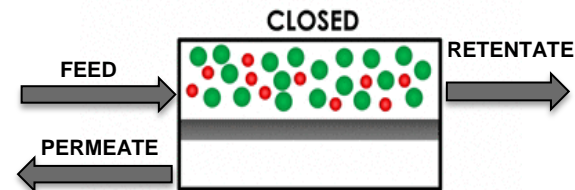


Separation performance of a pulsed retentate operation for different cycle times at constant productivity (opening to closing time ratio is 1/3).

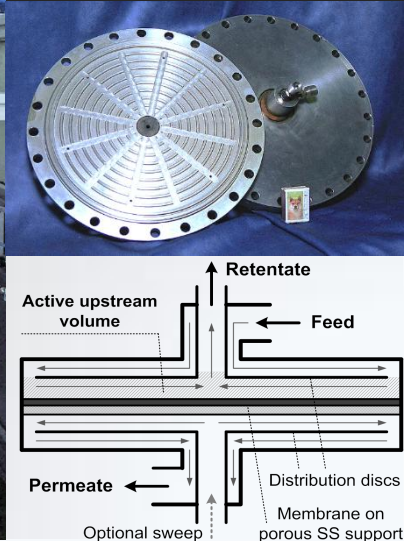
- SAME productivity
 - increasing amounts of withdrawn samples
- $\Delta\tau_{\text{open}}/\Delta\tau_{\text{total}} = 1/3$

NON-MONOTONIC DEPENDENCE

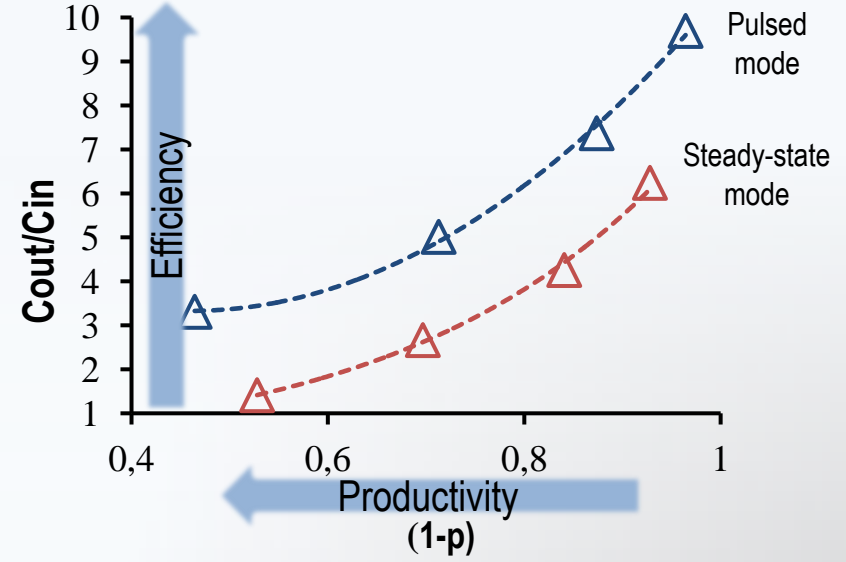
mutual influence of the amount of withdrawn sample and the stripping time



UNSTEADY-STATE MEMBRANE GAS SEPARATION WITH PERMEATE RECYCLE FOR LOW PERMEABLE COMPONENT CONCENTRATION SETUP



COMPARISON OF A PULSED MODE AND A STEADY-STATE MODE



Membrane – SILAR
 Pressure ratio – 1.1 bar
 Gas mixture – N₂O/N₂ = 99/1%

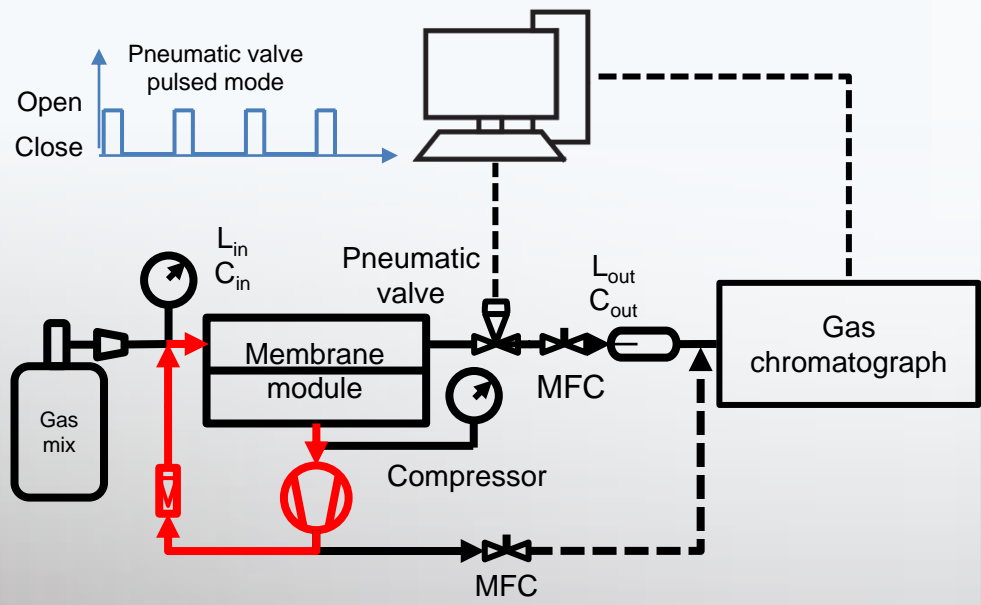
✓ Separation efficiency is higher for whole range of withdrawal rate
 Significant increase in separation efficiency at decreasing productivity

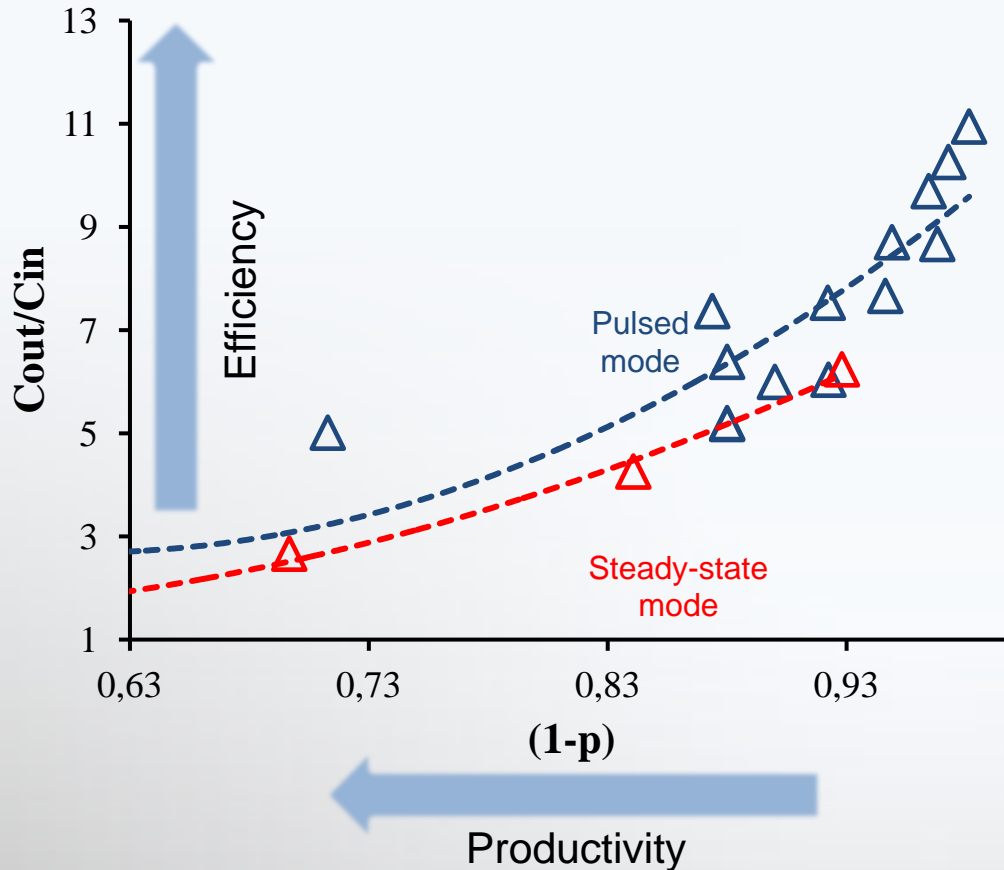
$$p = L_{out} / L_{in}$$

(1-p) = 1 ↓ **Minimum productivity**

(1-p) = 0 ↑ **Maximum productivity**

Principal scheme of unsteady-state membrane gas separation with permeate recycle for Low permeable component concentration setup

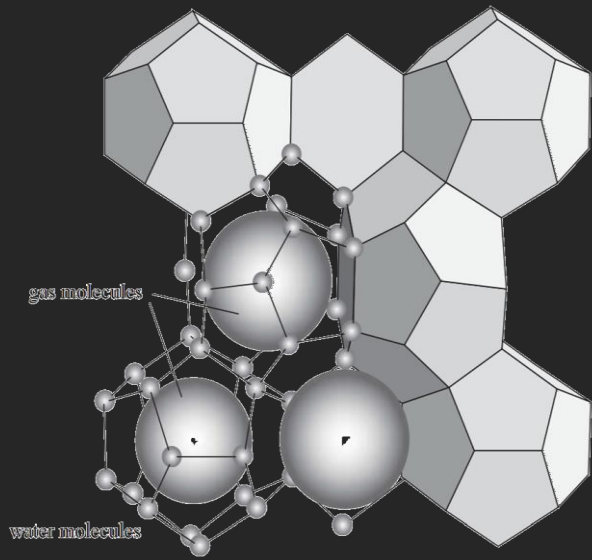




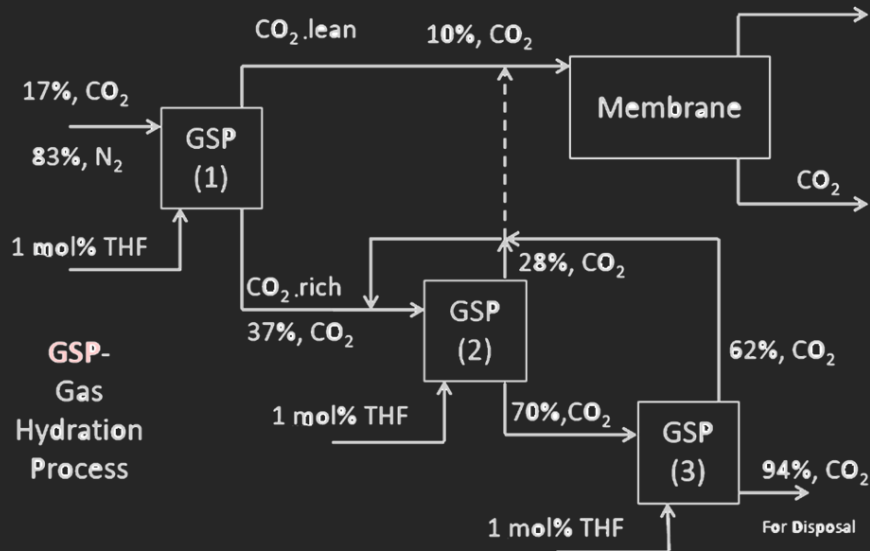
✓ Pulsed operation in permeate recycle mode with low permeable component concentration is more efficient in whole investigated range

✓ Optimization is required to determine most effective conditions of pulsed operation

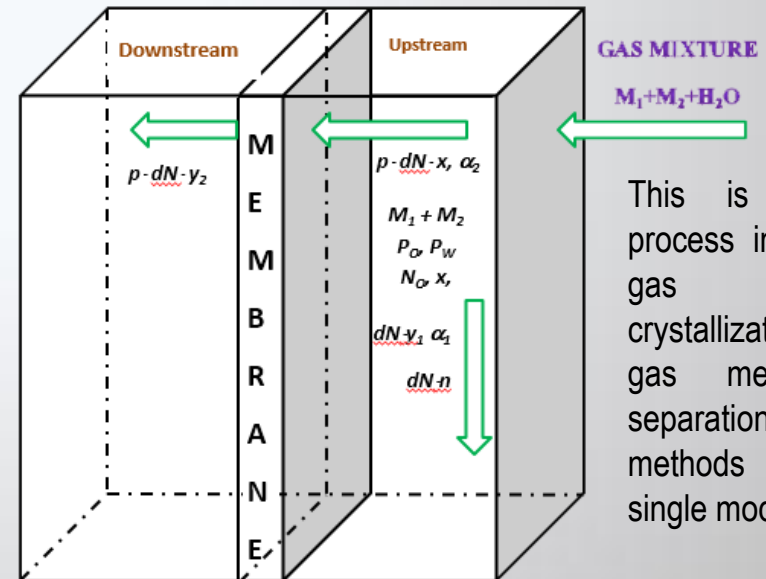
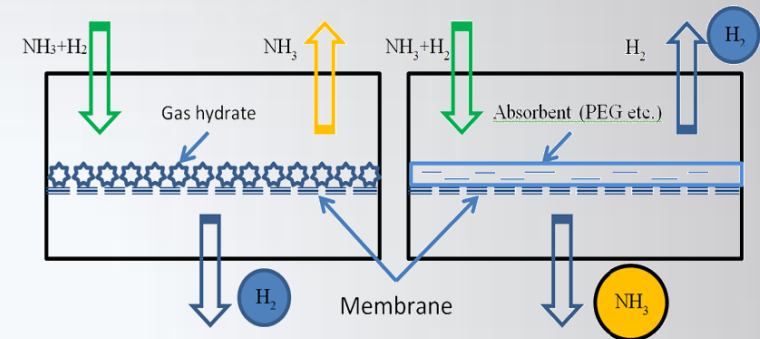
CASCADE OF MEMBRANE MODULE + GAS HYDRATE CRYSTALLIZATION



A hybrid hydrate-membrane process for CO₂ recovery from flue gas in the presence of THF as additive. Hydrate formation is carried out at 273.75 K and 2.5 MPa in the three stages.

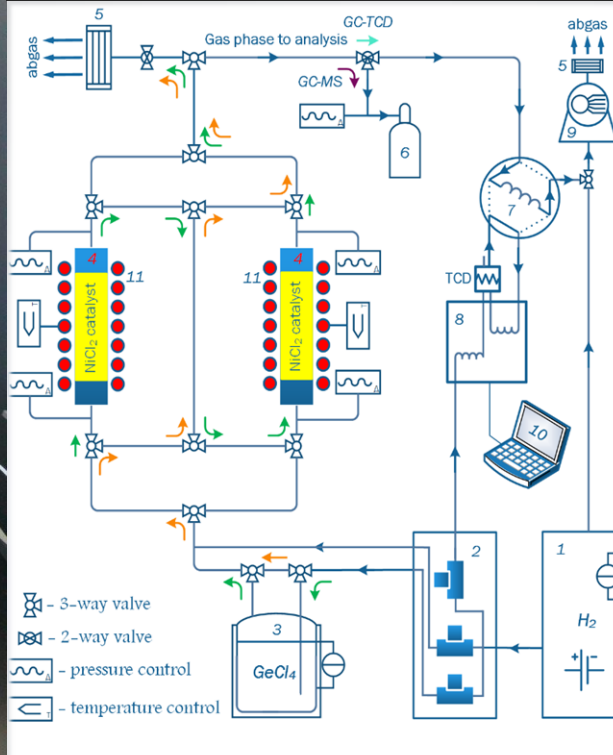


SCHEME OF THE HYBRID GAS HYDRATE-MEMBRANE SEPARATION METHOD



This is hybrid process including gas hydrate crystallization and gas membrane separation methods in the single module.

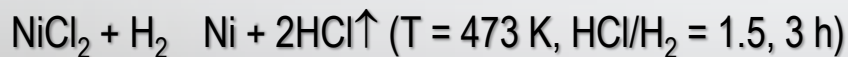
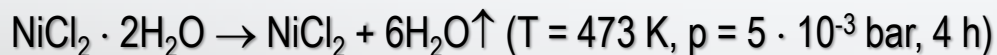
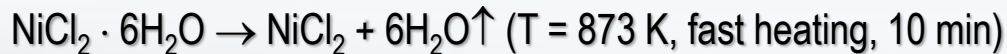
ENERGY SAVING CATALYTIC PROCESSES



CATALYST PREPARATION PROCEDURE



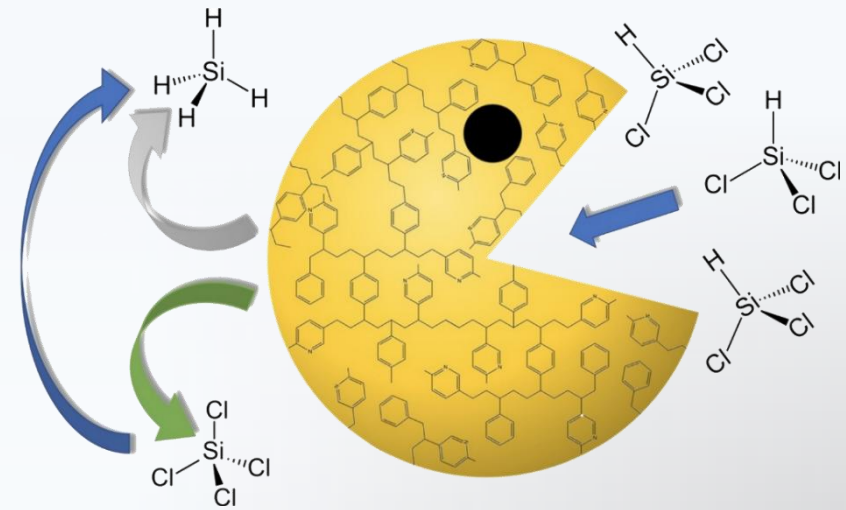
CATALYST PREPARATION PROCEDURE



Compound	Flammability	Explosive	Toxicity
SiCl ₄	1	2	4
GeCl ₄	1	2	4
SiHCl ₃	4	2	4
SiH ₄	4	3	2
GeH ₄	4	3	4

ENERGY SAVING CATALYTIC PROCESSES

REACTION MECHANISM



CHARACTERISTICS OF THE SYNTHESIZED CATALYST

Symbol	Diluents / (%v/v, Tol/Hep)	Specific area / $\text{m}^2 \cdot \text{g}^{-1}$	Average pore diameter / nm	Particle average diameter / μm	Exchange capacity / (meq/ml)
2M5VP-t	100/0	8.012	31.862	302	4.5
2M5VP-t/h	90/10	9.043	32.024	338	4.8
2M5VP-h/t	50/50	28.15	80.418	362	5.3

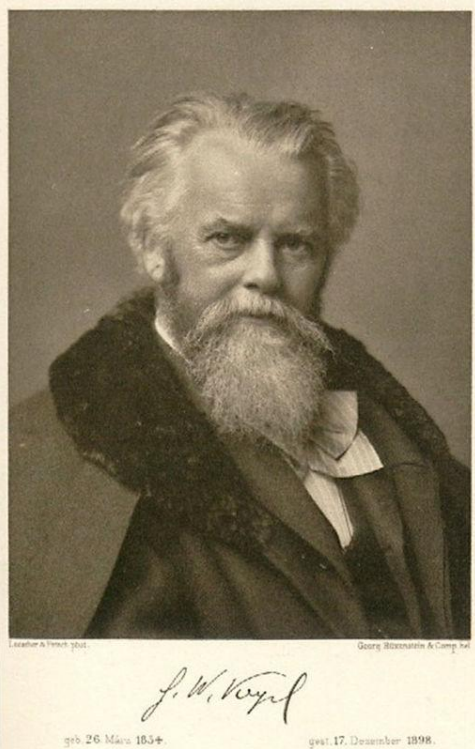
2M5VP-h/t

2M5VP-t

2M5VP-t/h

SEM micrographs of the 2M5VP resins with the different porogen

*Будучи химиком, Герман Фогель
знал, как сделать бомбу! На самом
деле большая часть его курса
обучения была посвящена тому, как
не сделать ее по ошибке...*



«Химия занимается веществами, а не телами»
Д.И. Менделеев



impossible



НИЖЕГОРОДСКИЙ ГОСУДАРСТВЕННЫЙ ТЕХНИЧЕСКИЙ УНИВЕРСИТЕТ им. Р.Е. Алексева ФЕДЕРАЛЬНЫЙ ОПОРНЫЙ УНИВЕРСИТЕТ

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